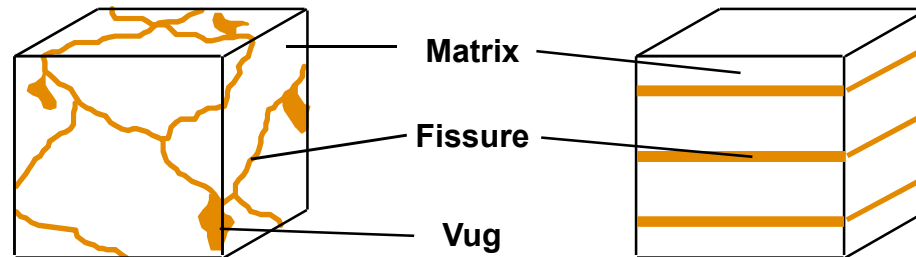
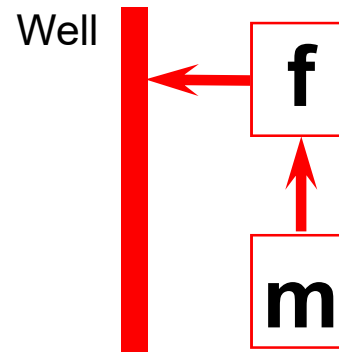


WELL TEST INTERPRETATION MODELS

NEAR WELLBORE EFFECTS	RESERVOIR BEHAVIOUR	BOUNDARY EFFECTS
Wellbore Storage Skin Fracture Partial Penetration Horizontal Well	Homogeneous Heterogeneous -2-Porosity -2-Permeability -Composite	Infinite extent Specified Rate Specified Pressure Leaky Boundary
EARLY TIMES	MIDDLE TIMES	LATE TIMES

DOUBLE POROSITY BEHAVIOUR



FISSURED

m matrix
f fissures

LAYERED

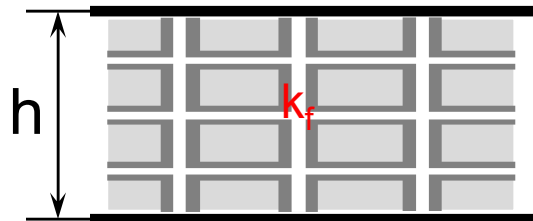
least permeable medium
most permeable medium

DOUBLE POROSITY BEHAVIOUR

Concentration of **f** or **m** : V_f (or V_m) = $\frac{\text{Volume of } f \text{ (or } m\text{)}}{\text{Total Bulk Volume}}$ $V_f + V_m = 1$

Porosity of **f** or **m** : ϕ_f (or ϕ_m) = $\frac{\text{Pore Volume of } f \text{ (or } m\text{)}}{\text{Volume of } f \text{ (or } m\text{)}}$ $\phi = \phi_f V_f + \phi_m V_m$

FISSURED

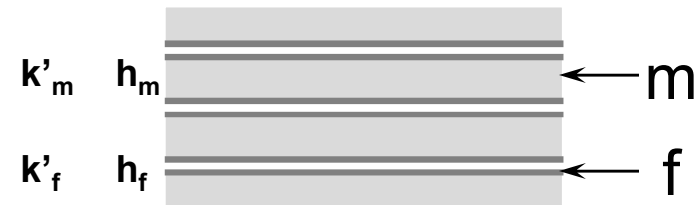


$$V_m \approx 1 \quad (V_f \ll V_m)$$

$$\phi_f \approx 1 \quad \phi = V_f + \phi_m$$

“Fissure” porosity (<0.01%)

LAYERED



$$V_f = \frac{h_f}{h_f + h_m} \quad V_m = \frac{h_m}{h_f + h_m}$$

$$\begin{aligned} k_f h &= k'_f h_f & k_f &= k'_f \frac{h_f}{h} = k'_f V_f \\ k_m h &= k'_m h_m & k_m &= k'_m \frac{h_m}{h} = k'_m V_m \end{aligned}$$

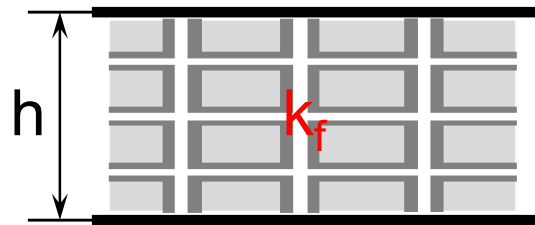
Effective vs intrinsic permeabilities

DOUBLE POROSITY BEHAVIOUR

Storativity ratio ω :

$$\omega = \frac{(\phi V c_t)_f}{(\phi V c_t)_f + (\phi V c_t)_m} = \frac{(\phi V c_t)_f}{(\phi V c_t)_{f+m}}$$

FISSURED



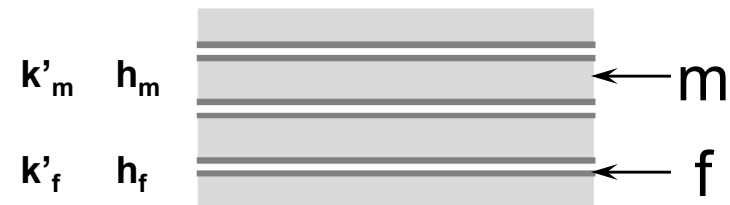
$$V_m \approx 1 \quad (V_f \ll V_m); \quad \phi_f \approx 1; \quad (c_t)_f \approx (c_t)_m$$

$$\omega \cong \frac{V_f}{V_f + \phi_m} \cong \frac{V_f}{\phi_m} \cong \frac{0.003}{0.3} = 0.01$$

Single phase: $\omega = 0.01 - 0.02$

Multiphase: $\omega = 0.1 - 0.2$

LAYERED



$$\omega \cong \frac{h_f \phi_f}{h_f \phi_f + h_m \phi_m}$$

$\omega = 0.1 - 0.2$

DOUBLE POROSITY BEHAVIOUR

Interporosity Flow Coefficient λ :

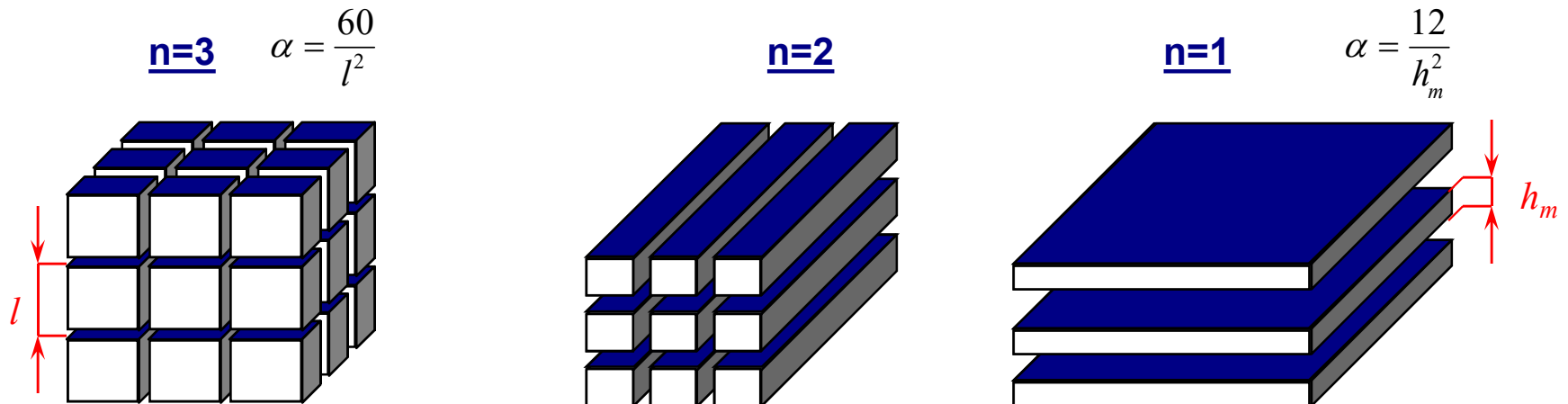
$$\lambda = \alpha r_w^2 \frac{k_m}{k_f}$$

α : geometric coefficient:

$$\alpha = \frac{4n(n+2)}{l^2}$$

n : number of directions of planes defining a matrix block

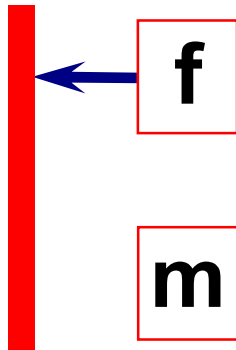
l : characteristic length of a matrix block



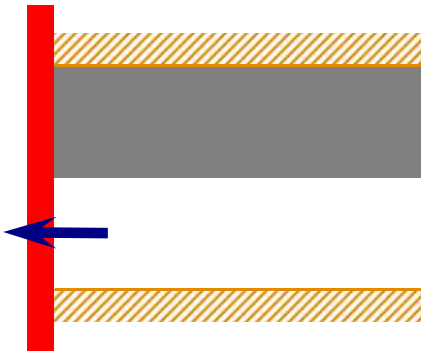
$$10^{-3} > \lambda > 10^{-7}$$

DOUBLE POROSITY BEHAVIOUR

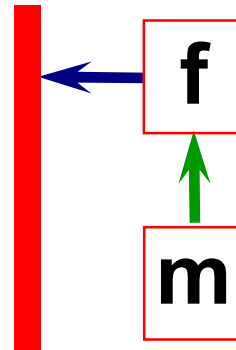
(1) EARLY TIMES



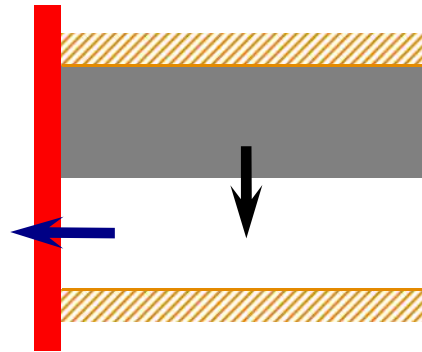
Flow from most permeable medium only



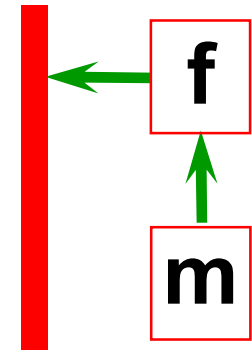
(2) TRANSITION



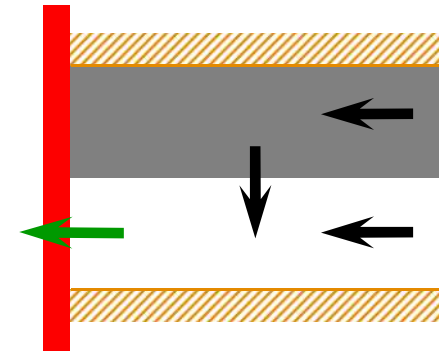
Recharge from least permeable medium



(3) LATER TIMES



Flow from both medium together



Double Porosity Behaviour

$$\tilde{p}_{wD}(C_{D_{f+m}}, S, s) = \frac{1}{s \left[s C_{D_{f+m}} + \frac{1}{\text{Skin} + \frac{K_0(\sqrt{s f(s)})}{\sqrt{s f(s)} K_1(\sqrt{s f(s)})}} \right]} = \frac{1}{s \left[s C_{D_{f+m}} + \frac{1}{\ln \frac{2}{e^\gamma \sqrt{s f(s)} e^{-2\text{Skin}}}} \right]}$$

$$s' = s C_{D_{f+m}} \text{ (call it } s) \Rightarrow p_{wD} \left[\left(\frac{t_D}{C_D} \right)_{f+m} \right] = \frac{1}{C_{D_{f+m}}} \tilde{p}_{wD}(s' C_{D_{f+m}}) \quad \gamma \text{ Euler's constant (} e^\gamma = 1.78 \text{)}$$

$$\tilde{p}_{wD} \left[(C_D e^{2\text{Skin}})_{f+m}, s \right] = \frac{1}{s \left[s + \frac{1}{\ln \frac{2}{e^\gamma \sqrt{s f(s)} / (C_D e^{2\text{Skin}})_{f+m}}} \right]}$$

Double Porosity Behaviour

Early times: $f(s) \approx \omega$ $\tilde{p}_{wD} \approx \tilde{p}_{wD_f} = \frac{1}{s \left[s + \frac{1}{\ln \frac{2}{e^\gamma \sqrt{\frac{s}{(C_D e^{2Skin})_f}}}} \right]}$

Late times: $f(s) \approx 1$ $\tilde{p}_{wD} \approx \tilde{p}_{wD_{f+m}} = \frac{1}{s \left[s + \frac{1}{\ln \frac{2}{e^\gamma \sqrt{\frac{s}{(C_D e^{2Skin})_{f+m}}}}} \right]}$

Intermediate times: $s f(s) \approx \lambda C_{D_{f+m}}$ $\tilde{p}_{wD} \approx \frac{1}{s \left[s + \frac{1}{\ln \frac{2}{e^\gamma \sqrt{\lambda e^{-2Skin}}}} \right]}$

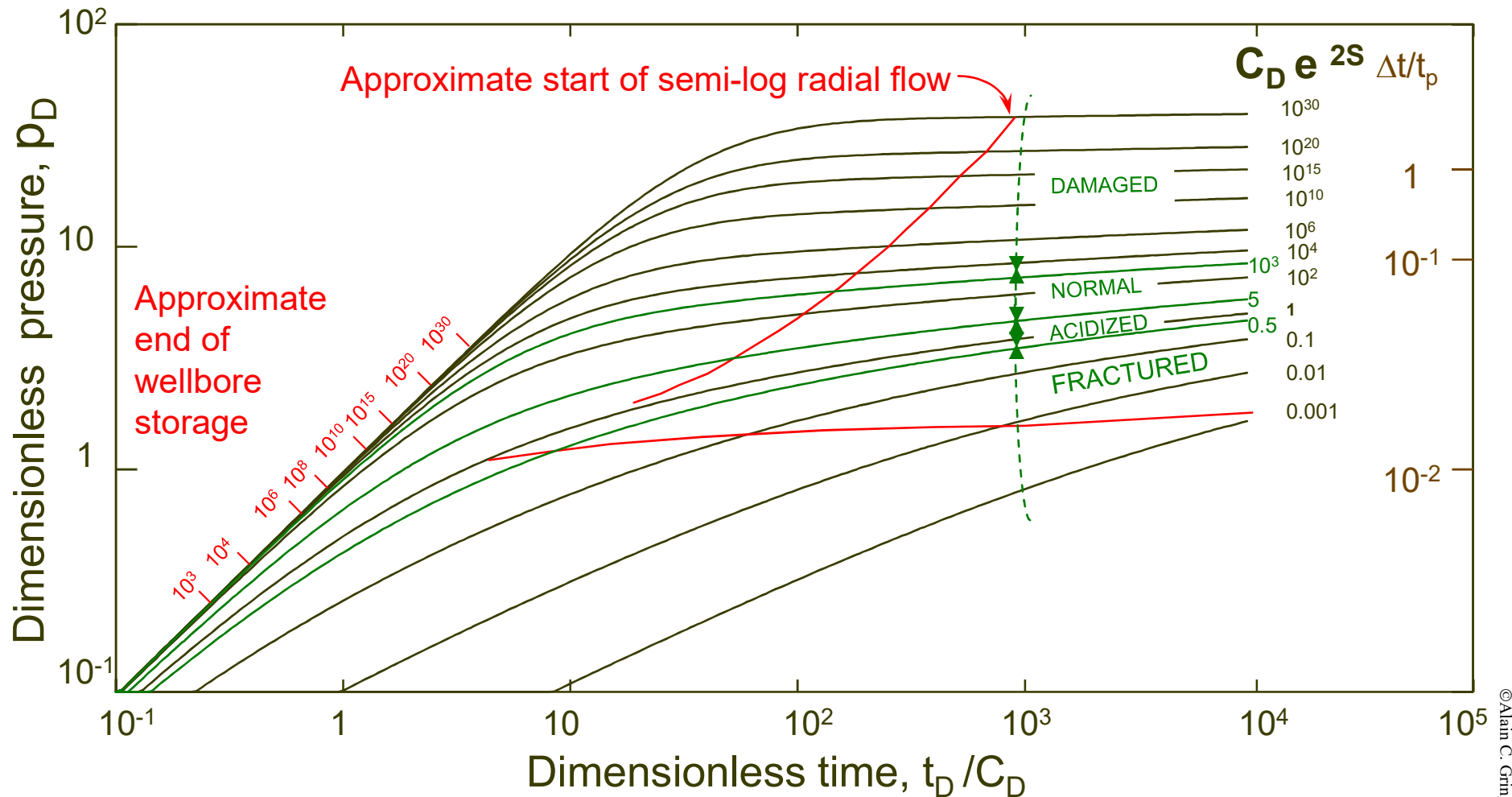
$$p_D, \frac{t_D}{C_D}, C_D e^{2Skin}, \omega, \lambda e^{-2Skin}$$

Independent variables (Bourdet and Gringarten, 1980)

DOUBLE POROSITY BEHAVIOUR

Parameter	Early Times	Later Times
<i>Medium</i>	f	$f+m$
<i>Permeability-thickness</i>	$k_f h$	$k_f h$
<i>Storativity</i>	$(\phi V c_t)_f h$	$(\phi V c_t)_{f+m} h$
<i>Dimensionless pressure</i>	$p_D = \frac{k_f h}{141.2 q B \mu} \Delta p$	<i>Same</i>
<i>Dimensionless time</i>	$t_{Df} = \frac{0.000264 k_f}{(\phi V c_t)_f \mu r_w^2} \Delta t$	$t_{Df+m} = \frac{0.000264 k_f}{(\phi V c_t)_{f+m} \mu r_w^2} \Delta t$
<i>Dimensionless wellbore storage</i>	$C_{Df} = \frac{0.8936 C}{(\phi V c_t)_f h r_w^2}$	$C_{Df+m} = \frac{0.8936 C}{(\phi V c_t)_{f+m} h r_w^2}$
<i>Skin</i>	S	S
$\frac{t_D}{C_D}$	$\frac{t_{Df}}{C_{Df}} = 0.000295 \frac{k_f h}{\mu} \frac{\Delta t}{C}$	$\frac{t_{Df+m}}{C_{Df+m}} = \frac{t_{Df}}{C_{Df}} = 0.000295 \frac{k_f h}{\mu} \frac{\Delta t}{C}$
$C_D e^{2S}$	$(C_D e^{2S})_f = \frac{0.8936 C e^{2S}}{(\phi V c_t)_f h r_w^2}$	$(C_D e^{2S})_{f+m} = \frac{0.8936 C e^{2S}}{(\phi V c_t)_{f+m} h r_w^2} = \omega (C_D e^{2S})_f$
$PM = \left(\frac{p_D}{\Delta p} \right)_{match}$	$\frac{k_f h}{141.2 q B \mu}$	<i>Same</i>
$TM = \left(\frac{t_D / C_D}{\Delta t} \right)_{match}$	$0.000295 \frac{k_f h}{\mu} \frac{1}{C}$	<i>Same</i>
λ	λe^{-2S}	<i>Same</i>

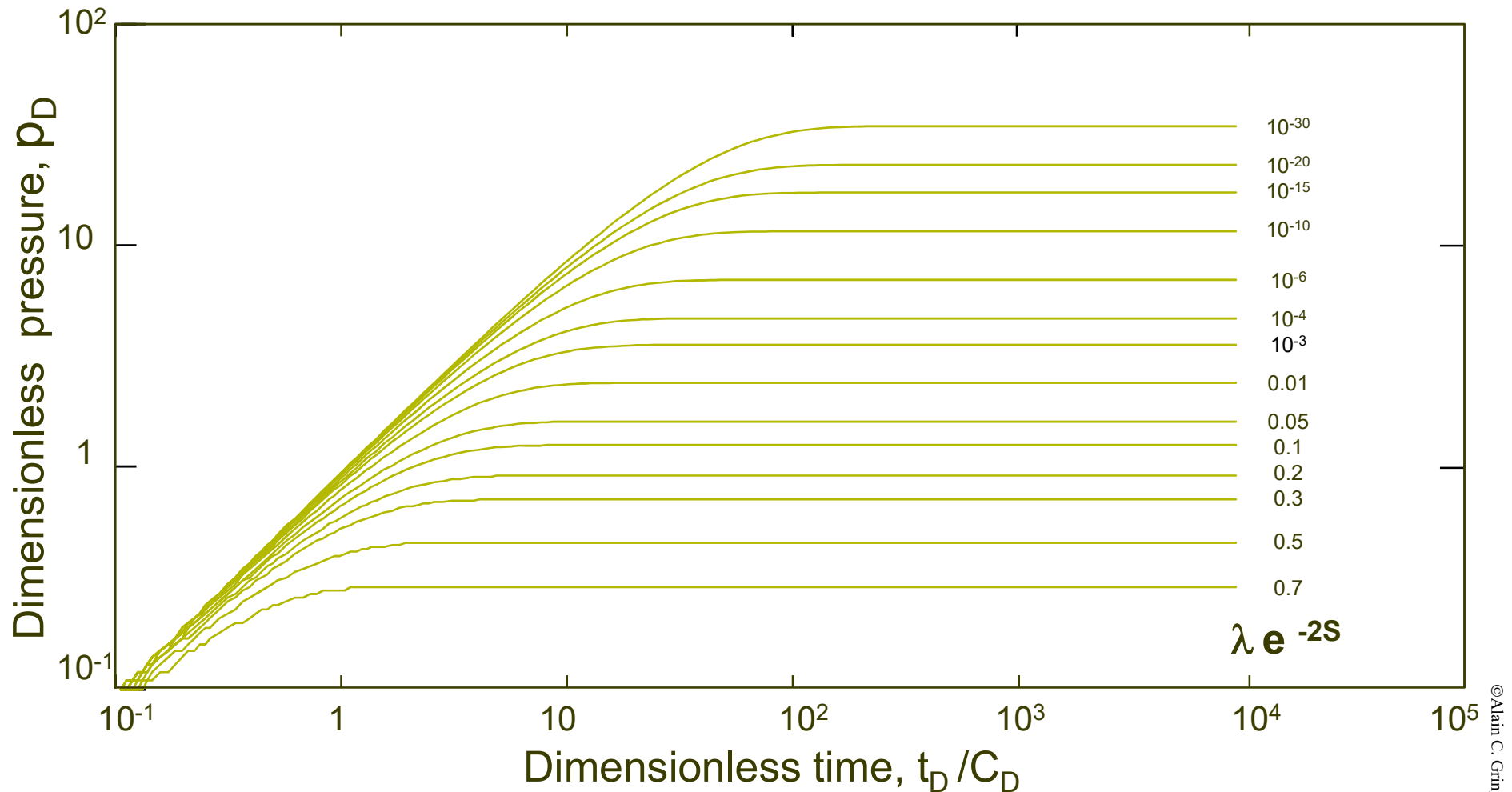
EARLY AND LATER TIMES DOUBLE POROSITY BEHAVIOUR: Wellbore Storage and Skin Type curve



$$p_D = \frac{kh}{141.2 \Delta q B \mu} \Delta p \quad \frac{t_D}{C_D} = 0.000295 \frac{kh}{\mu C} \Delta t \quad C_D e^{2S} = \frac{0.8936}{\phi c_t h r_w^2} C e^{2S}$$

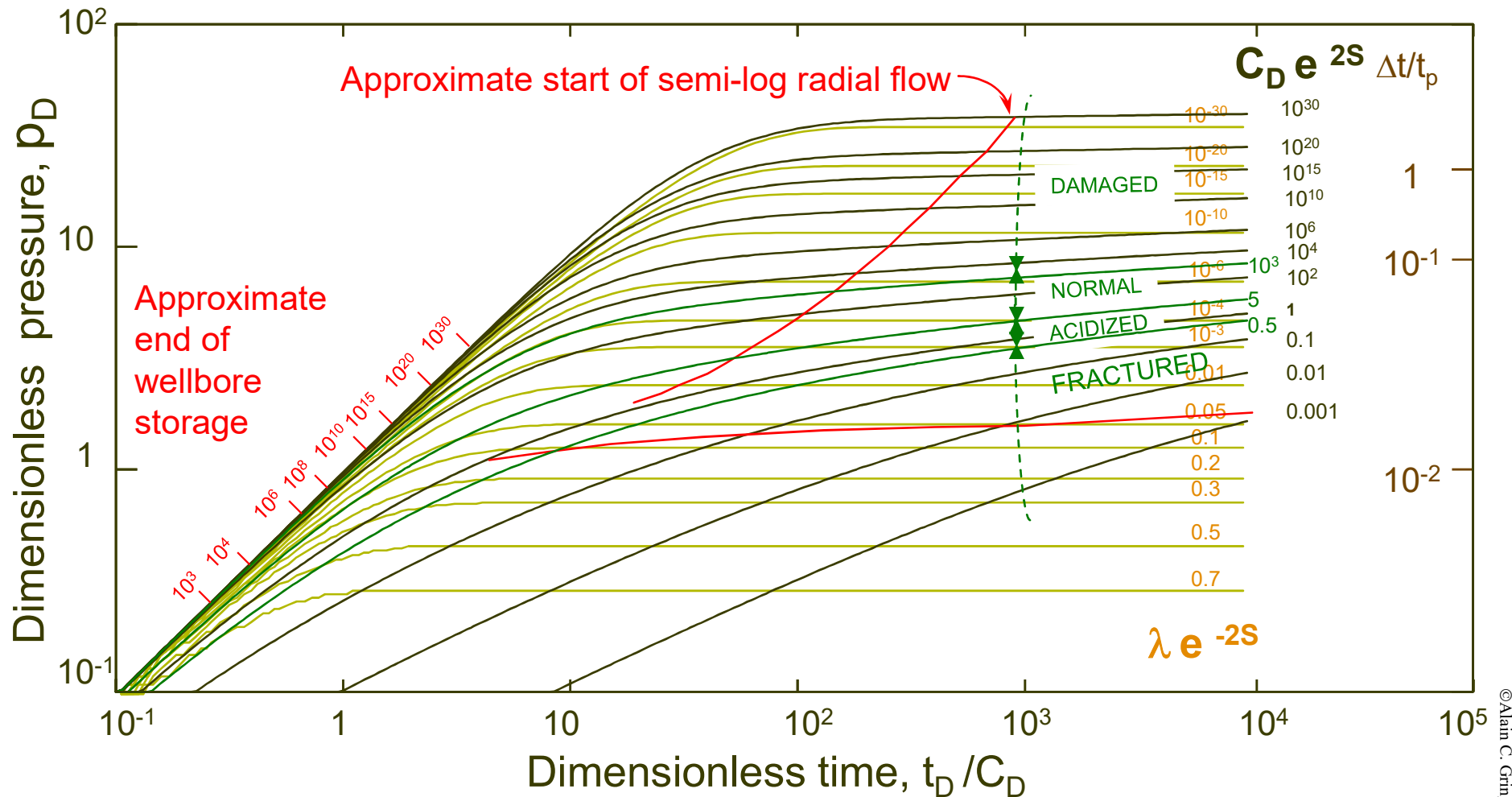
INTERMEDIATE TIMES DOUBLE POROSITY BEHAVIOUR:

λe^{-2s} Transition Type Curve



$$p_D = \frac{kh}{141.2\Delta q B\mu} \Delta p \quad \frac{t_D}{C_D} = 0.000295 \frac{kh}{\mu C} \Delta t \quad \lambda e^{-2s} = \alpha r_w^2 \frac{k_m}{k_f} e^{-2s}$$

Drawdown Type Curve for a Well with Wellbore Storage & Skin, in a Reservoir of Infinite Extent with Double Porosity Behaviour (Restricted Interporosity Flow)

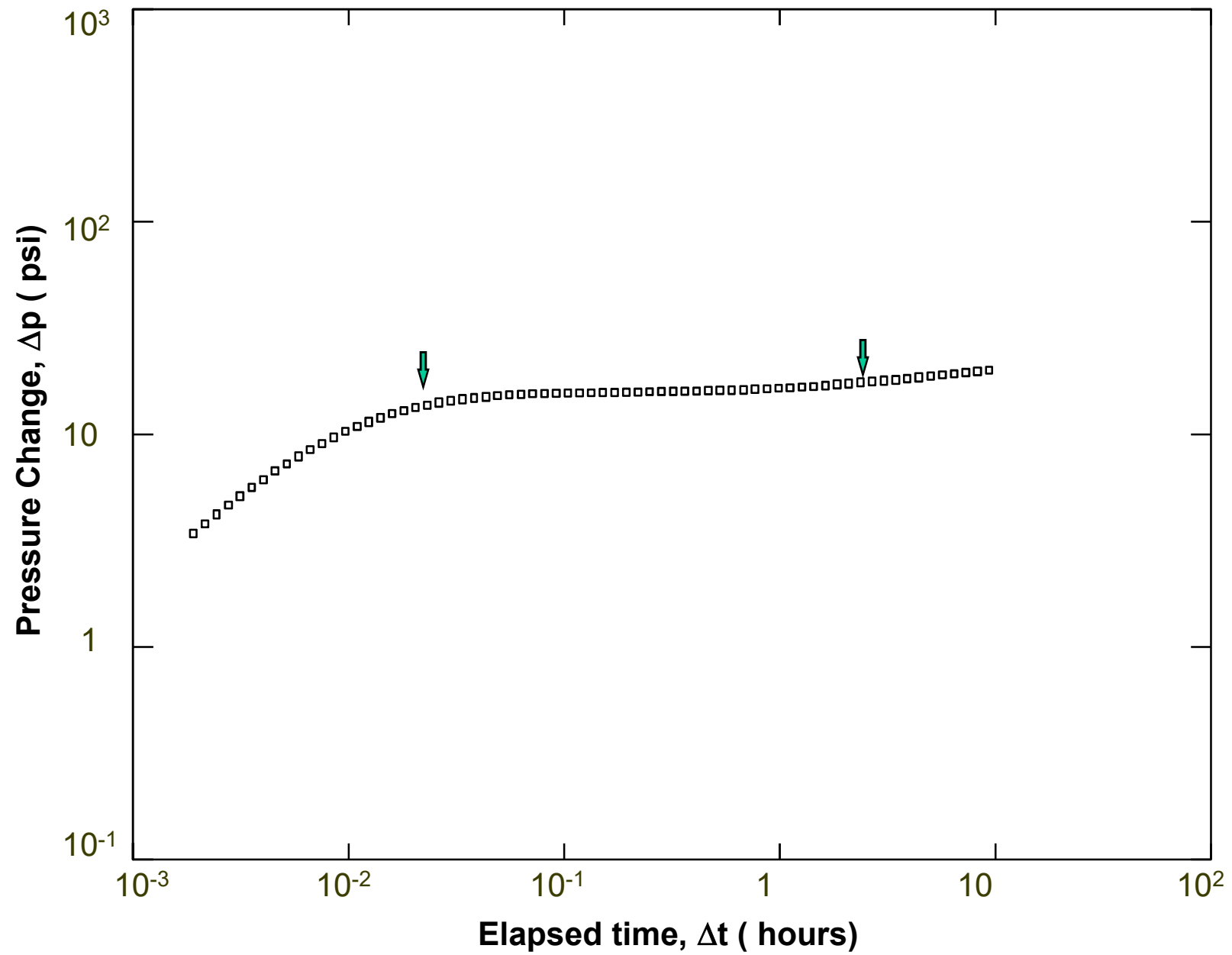


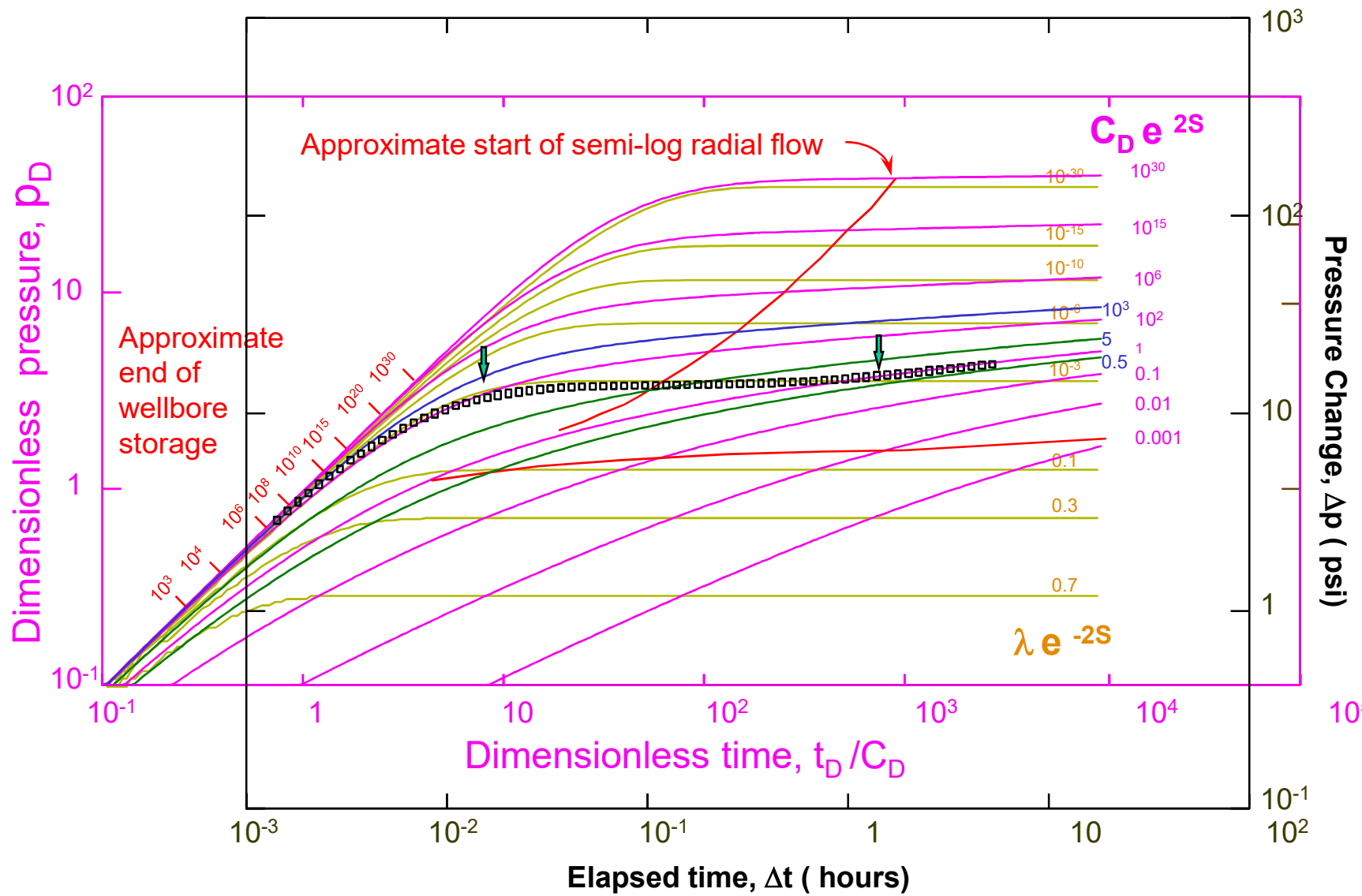
SPE 9293
Type Curve

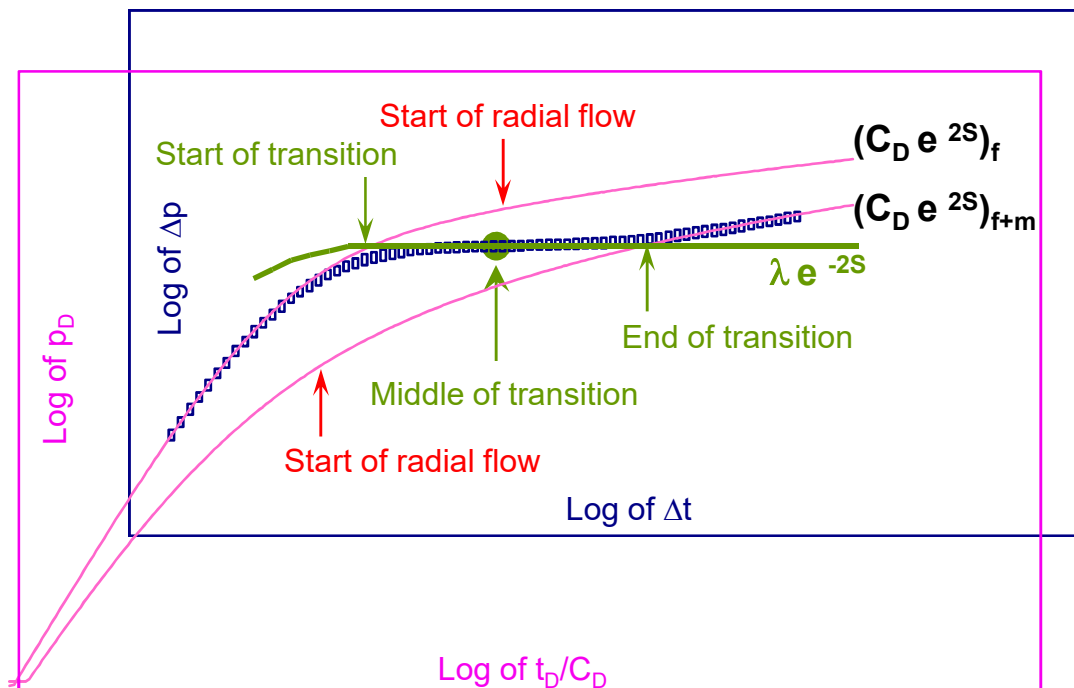
$$p_D = \frac{kh}{141.2\Delta q B\mu} \Delta p$$

$$\frac{t_D}{C_D} = 0.000295 \frac{kh}{\mu C} \Delta t$$

$$C_D e^{2S} = \frac{0.8936}{\phi c_t h r_w^2} C e^{2S}$$







PRESURE MATCH:

$$PM = \left(\frac{p_D}{\Delta p} \right)_{match}$$

TIME MATCH:

$$TM = \left(\frac{t_D / C_D}{\Delta t} \right)_{match}$$

CURVE MATCHES:

$$(C_D e^{2S})_f$$

$$(C_D e^{2S})_{f+m}$$

$$\lambda e^{-2S}$$

$$kh = 141.2 \Delta q B \mu PM$$

$$C = 0.000295 \frac{kh}{\mu} \left(\frac{1}{TM} \right)$$

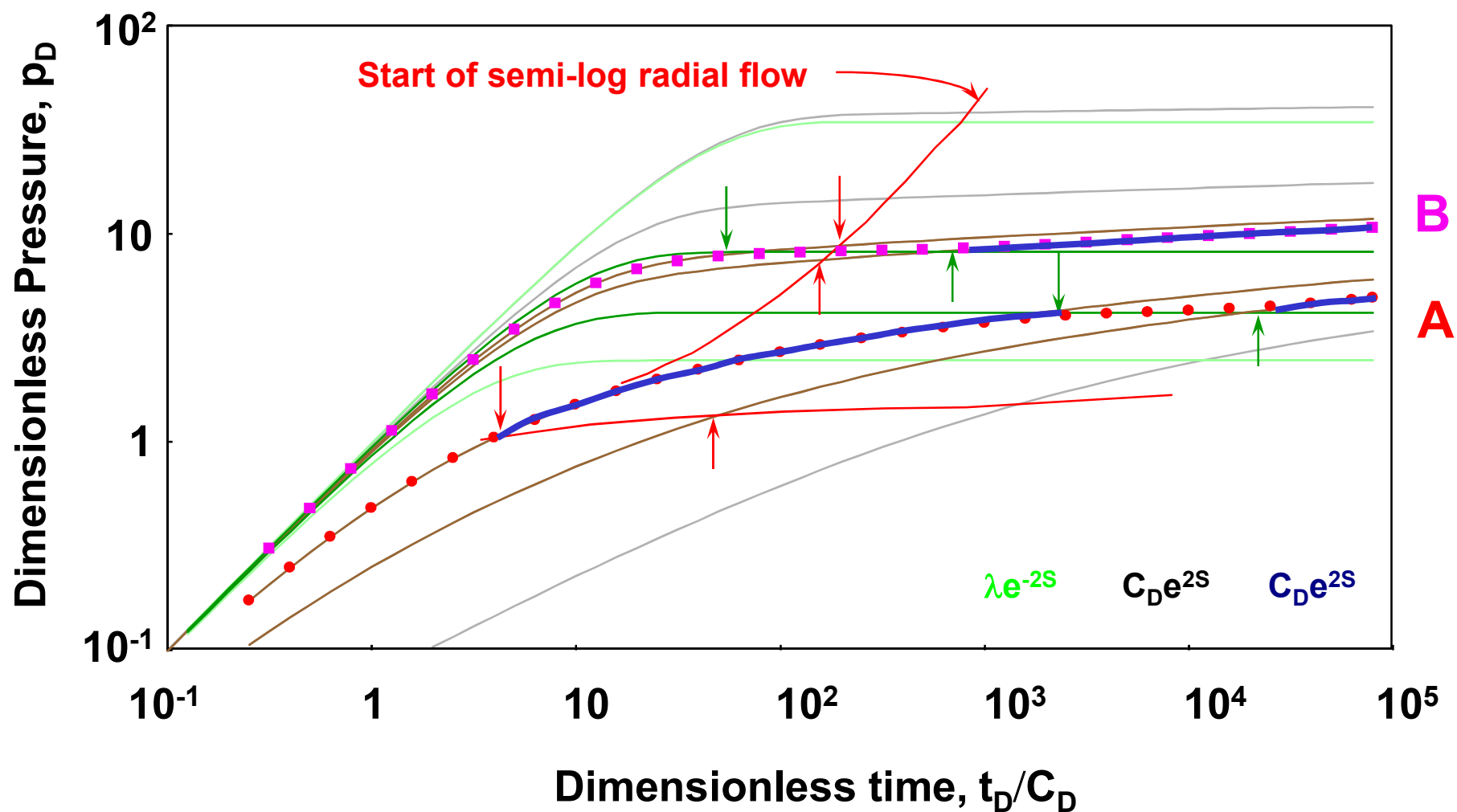
$$\omega = \frac{(C_D e^{2S})_{f+m}}{(C_D e^{2S})_f}$$

$$S = 0.5 \ln \frac{(C_D e^{2S})_f}{C_{Df}} = 0.5 \ln \frac{(C_D e^{2S})_{f+m}}{C_{Df+m}}$$

$$\lambda = (\lambda e^{-2S}) e^{2S}$$

$$C_{Df} = \frac{0.8936C}{(\phi V c_t)_f h r_w^2} \quad (\phi V c_t)_f = \frac{\omega}{1 - \omega} (\phi c_t)_m$$

$$C_{Df+m} = \frac{0.8936C}{(\phi V c_t)_{f+m} h r_w^2} \quad (\phi V c_t)_{f+m} = \frac{1}{1 - \omega} (\phi c_t)_m$$



↓ Start of radial flow on fissure medium $(C_D e^{2S})_f$ curve

↑ Start of radial flow on total system $(C_D e^{2S})_{f+m}$ curve

↓ Start of transition on fissure medium $(C_D e^{2S})_f$ curve

↑ End of transition on total system $(C_D e^{2S})_{f+m}$ curve

Existence of double porosity semi-log straight lines (drawdown)

1st line: Data must match $(C_D e^{2S})_f$

after the start of radial flow on (f)
before the start of transition

2nd line: Data must match $(C_D e^{2S})_{f+m}$

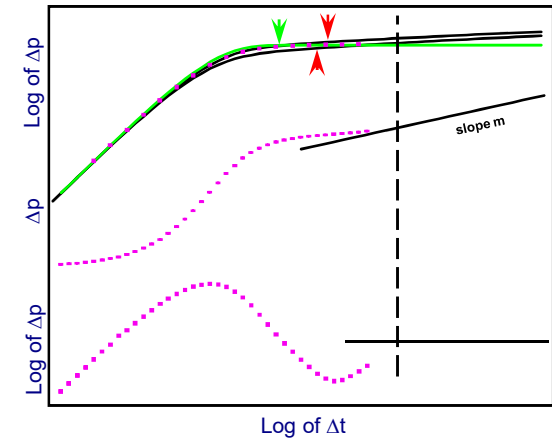
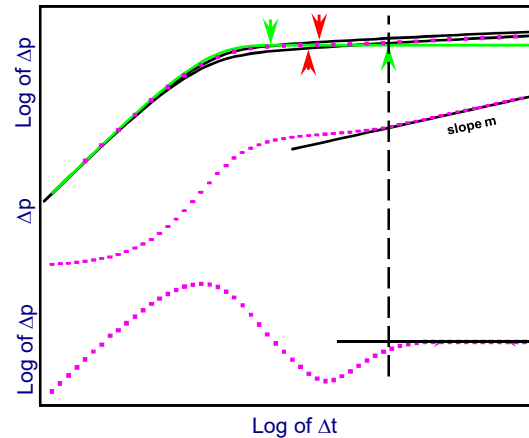
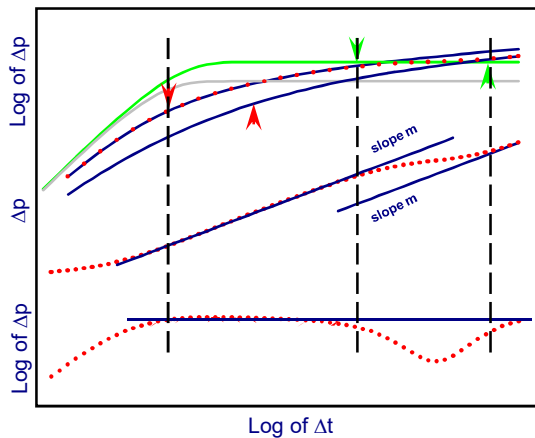
after the end of transition
after the start of radial flow on (f+m)

POSSIBILITY OF:

2 straight lines

1 straight line

0 straight line



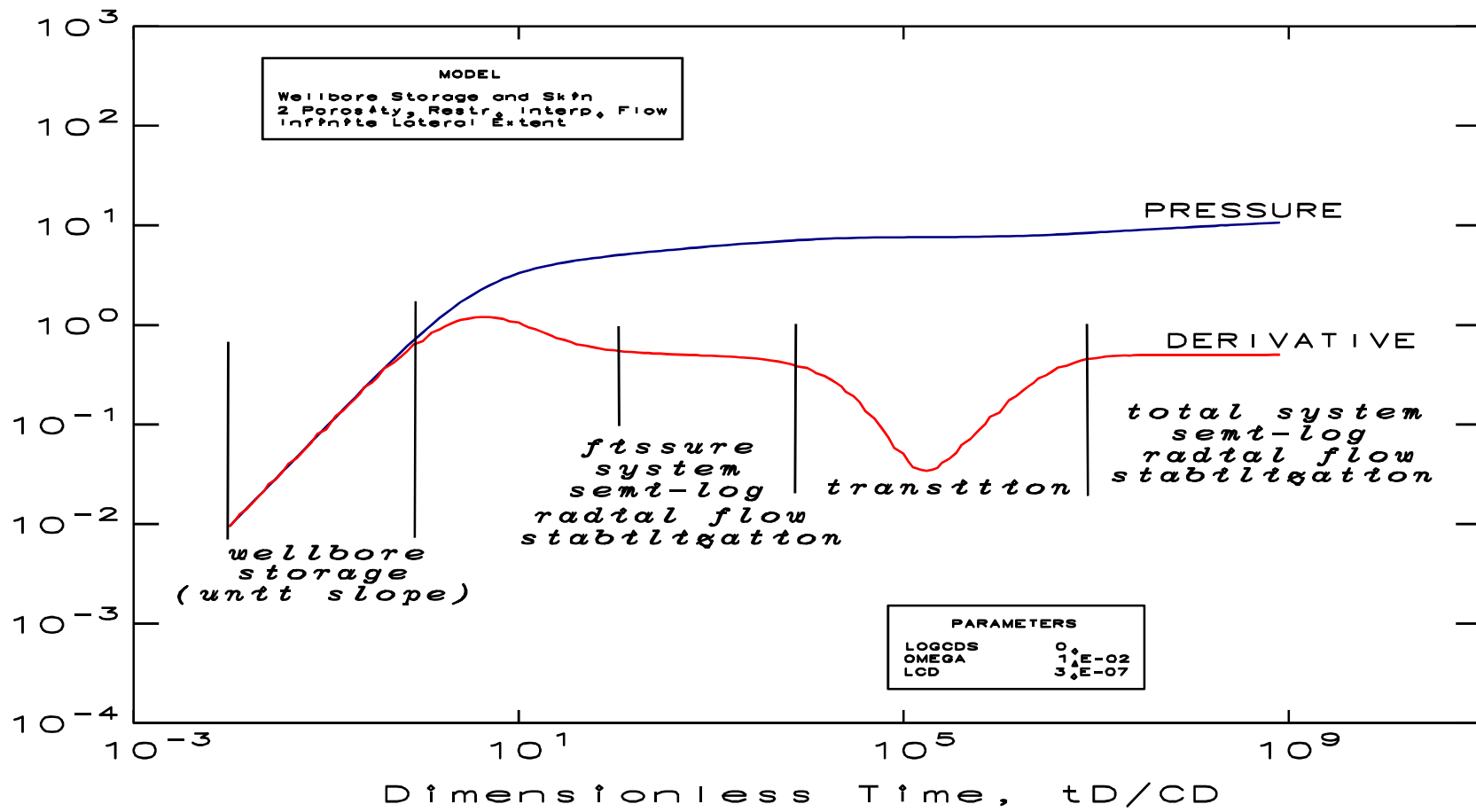
DEPENDING UPON:

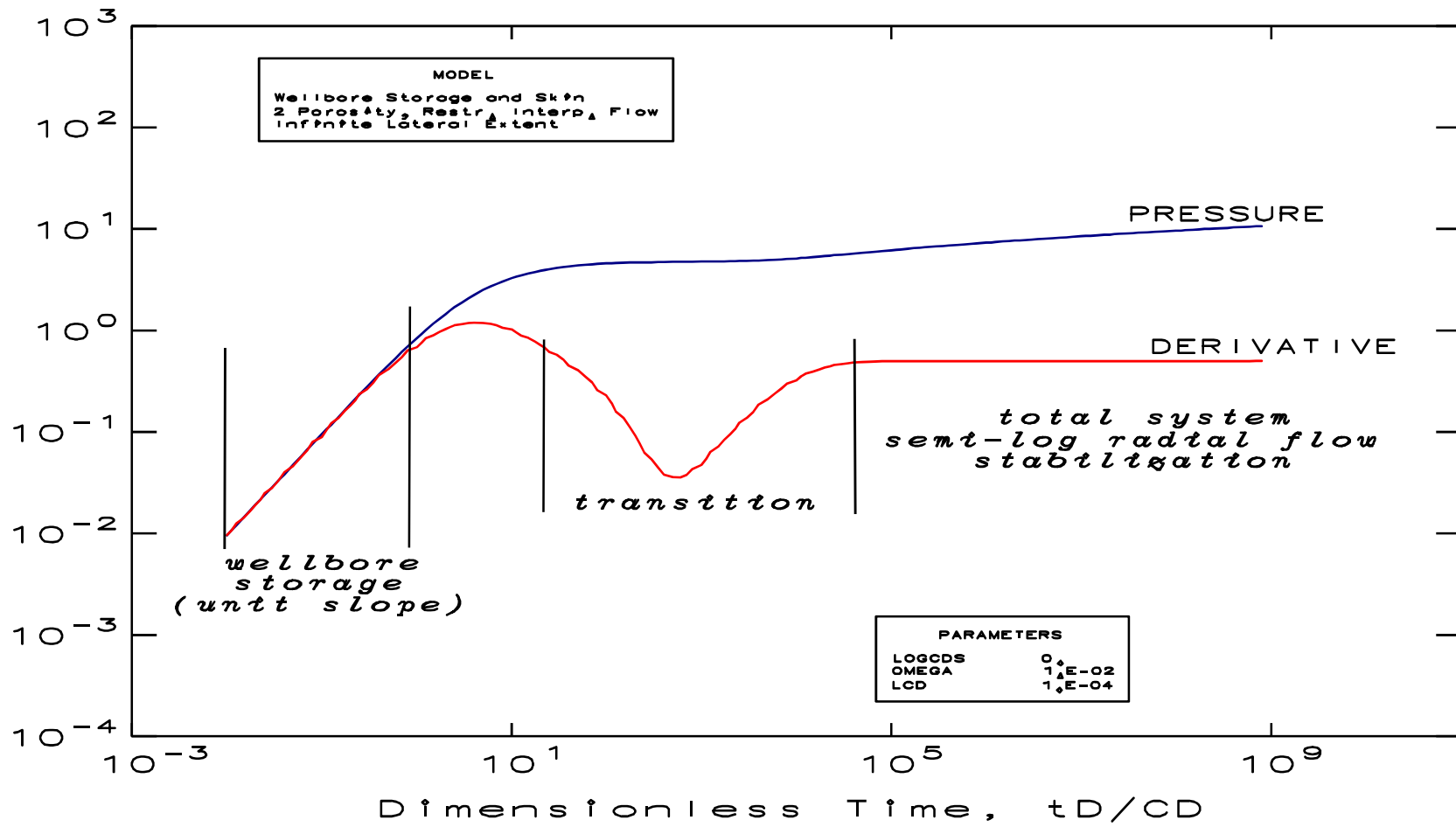
i.e.: $(C_D e^{2S})_f$
 $S, (c_t)_f$

condition of well & behaviour of fluid

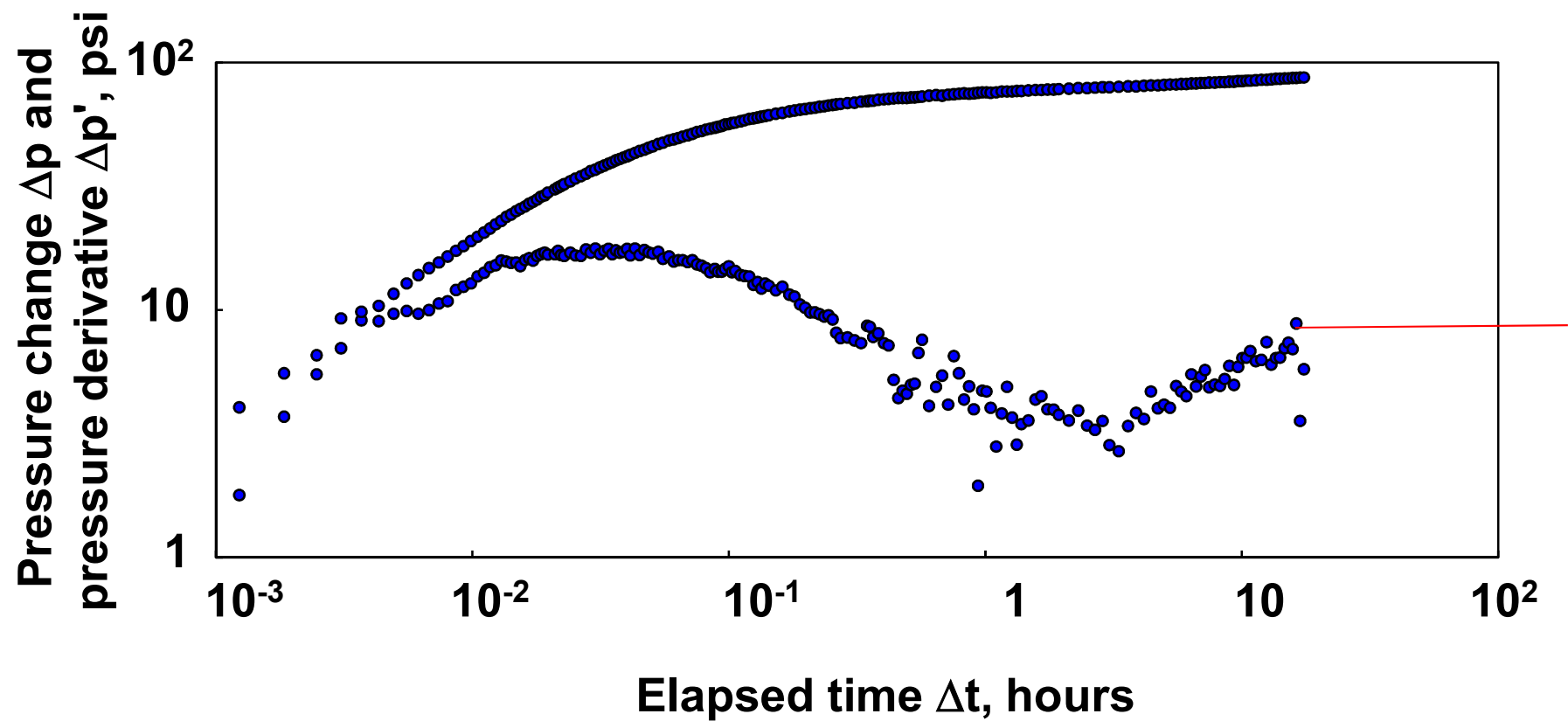
$(C_D e^{2S})_{f+m}$
 $S, (c_t)_{f+m}$

λe^{-2S}
 S, k_m

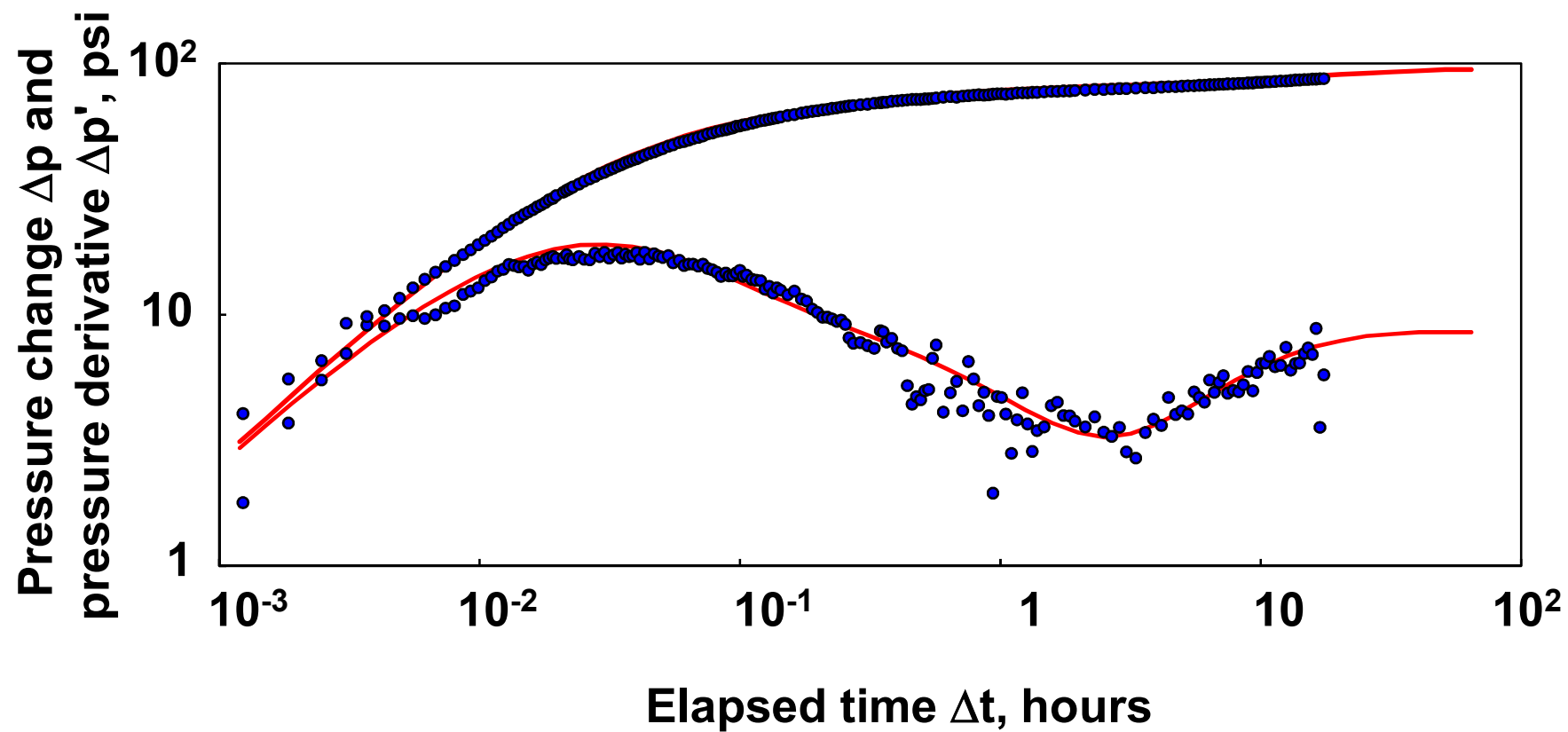




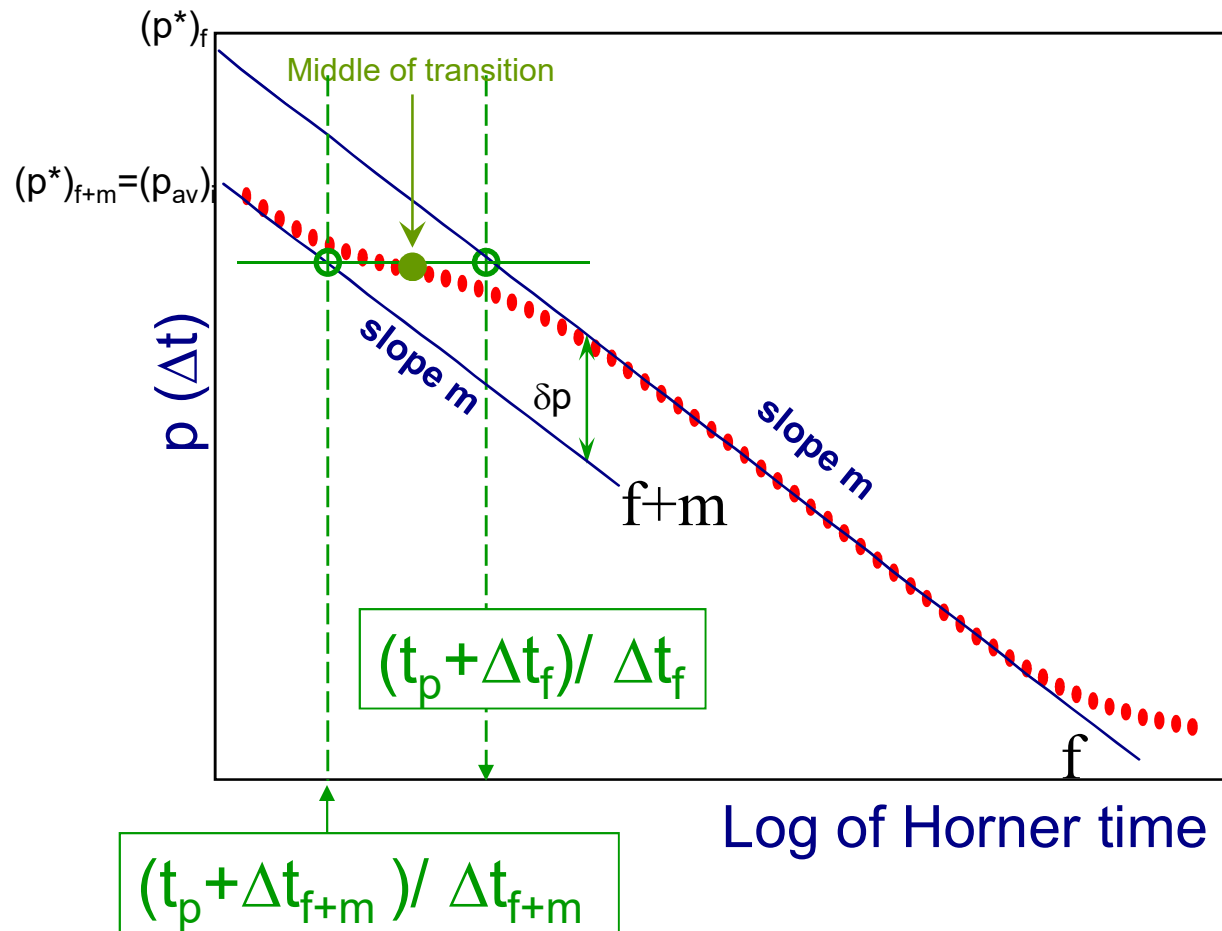
EXAMPLE OF DOUBLE POROSITY BEHAVIOUR



EXAMPLE OF DOUBLE POROSITY BEHAVIOUR



DOUBLE POROSITY SEMI-LOG Horner ANALYSIS



Radial flow (f) and (f+m) lines:

m δp

Transition line:

$(\Delta t)_f$ $(\Delta t)_{f+m}$

$$kh = 162.6 \Delta q B \mu \frac{1}{m} \quad \omega = 10^{-\delta p / m}$$

$$\lambda = \frac{(\phi V c_t)_f \mu r_w^2}{0.000264 \gamma k_f (\Delta t_f)} = \frac{(\phi V c_t)_{f+m} \mu r_w^2}{0.000264 \gamma k_f (\Delta t_{f+m})} \quad \gamma = 1.78 \text{ Exponential of Euler constant}$$



$$PM = \left(\frac{p_D}{\Delta p} \right)_{match}$$

TIME MATCH:

$$TM = \left(\frac{t_D / C_D}{\Delta t} \right)_{match}$$

CURVE MATCHES:

$$\begin{pmatrix} C_D e^{2S} \end{pmatrix}_f$$

$$\begin{pmatrix} C_D e^{2S} \end{pmatrix}_{f+m}$$

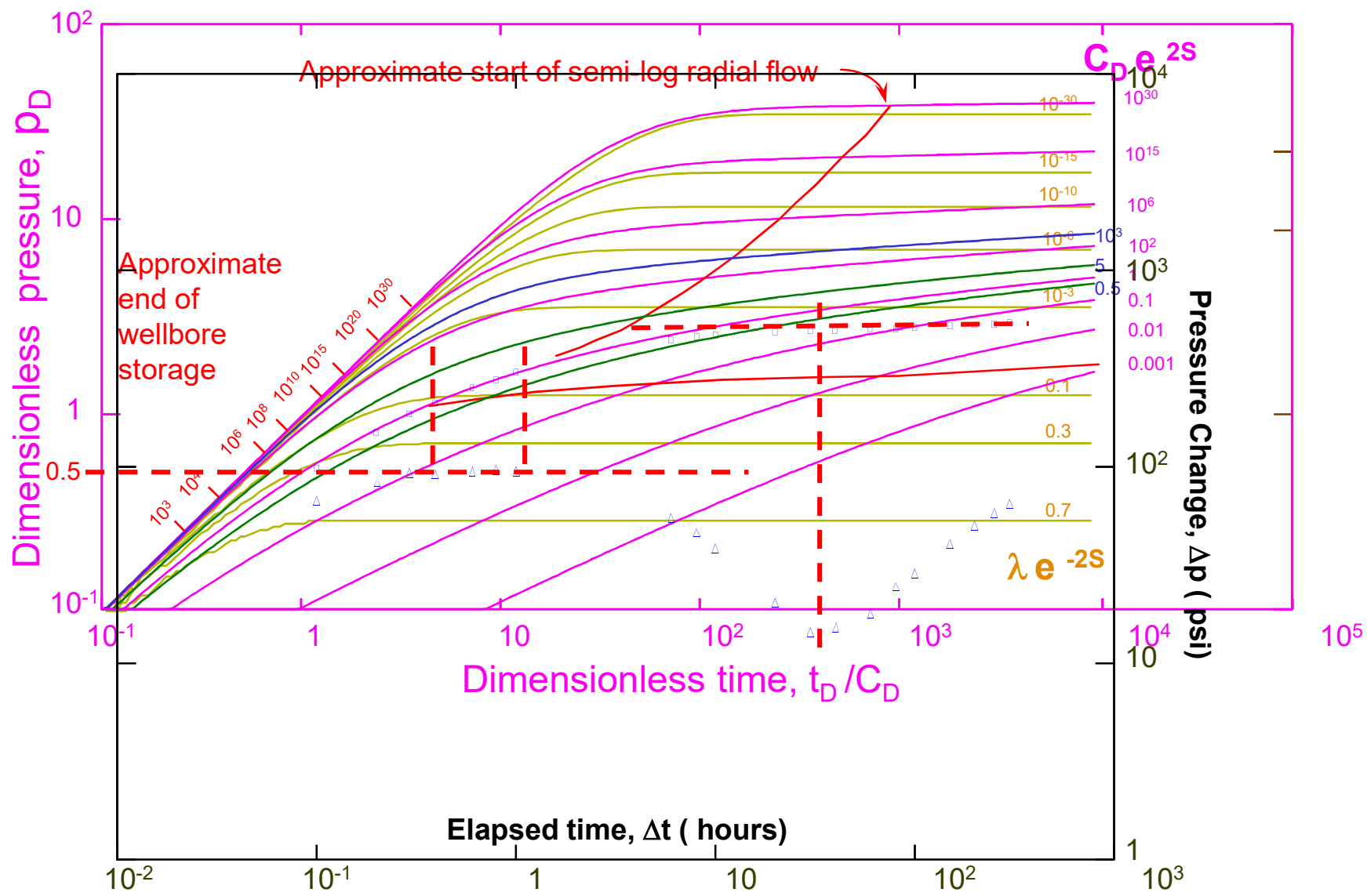
$$\frac{\lambda(C_D)_{f+m}}{1-\omega} \qquad \frac{\lambda(C_D)_{f+m}}{\omega(1-\omega)}$$

$$kh = 141.2 \Delta q B \mu \text{ PM}$$

$$C = 0.000295 \frac{kh}{\mu} \left(\frac{1}{\text{TM}} \right)$$

$$\omega = \frac{\lambda(C_D)_{f+m} / (1-\omega)}{\lambda(C_D)_{f+m} / \omega(1-\omega)} \longrightarrow C_{Df+m} = (1-\omega) C_{Dm} \longrightarrow S = 0.5 \ln \frac{(C_D e^{2S})_{f+m}}{C_{Df+m}} = 0.5 \ln \frac{(C_D e^{2S})_f}{C_{Df}}$$

$$\lambda = (1 - \omega) \left(\lambda(C_D)_{f+m} / (1 - \omega) \right) / (C_D)_{f+m}$$

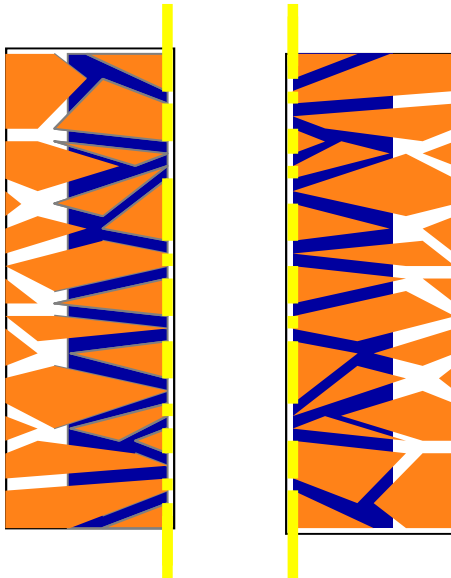


DOUBLE POROSITY BEHAVIOUR

	Fissured	Multilayered	Homogeneous
DAMAGED	C normal	C normal	C normal 0.01 Bbl/psi
$(C_D e^{2S})_f > 10^3$	$S > -3.5$	$S > -3.5$	$S > 0$
ACIDISED	C 10-100 Times normal	C normal	C normal
$0.5 < (C_D e^{2S})_f < 5$	S as low as -7	S as low as -7	S as low as -4
FRACTURED	C normal	C normal	C normal
$(C_D e^{2S})_f < 0.5$	$S \approx -5.5$	$S \approx -5.5$	$S \approx -5.5$

DOUBLE POROSITY BEHAVIOUR

Damaged



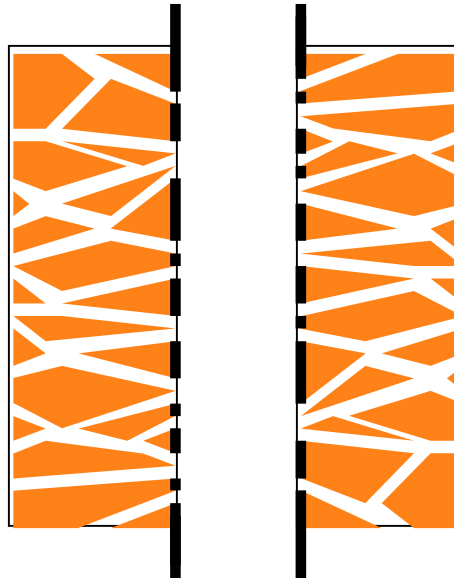
**Fissures
Plugged**

C normal

$S > -3.5$

Skin = -3.5 = "Geo-skin"

Acidised



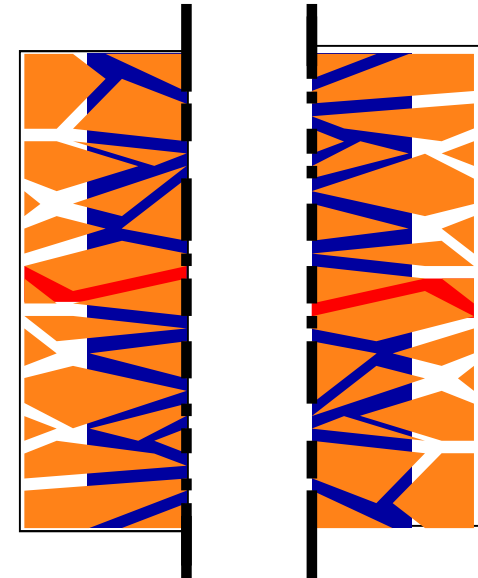
**Fissures
Cleaned Open**

C 10-100 normal

S as low as -7

Skin = Geoskin - 4

Fractured



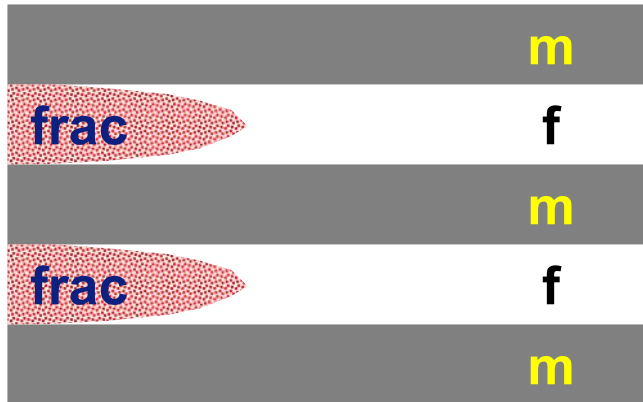
**Fracture propagates
along existing fissures**

C normal

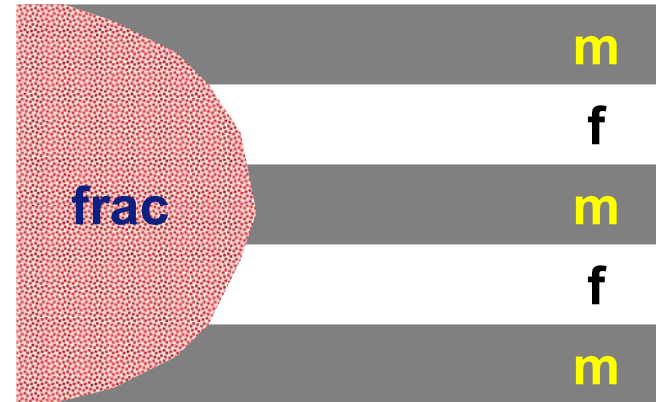
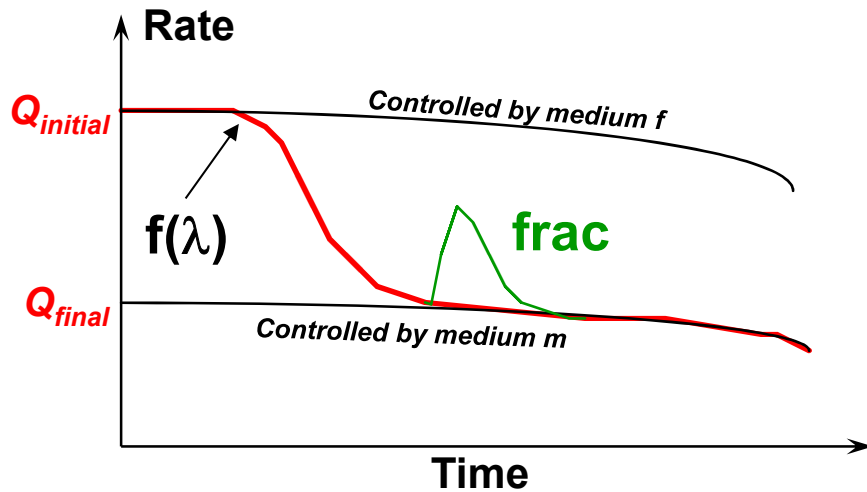
$S \approx -5.5$

DOUBLE POROSITY BEHAVIOUR

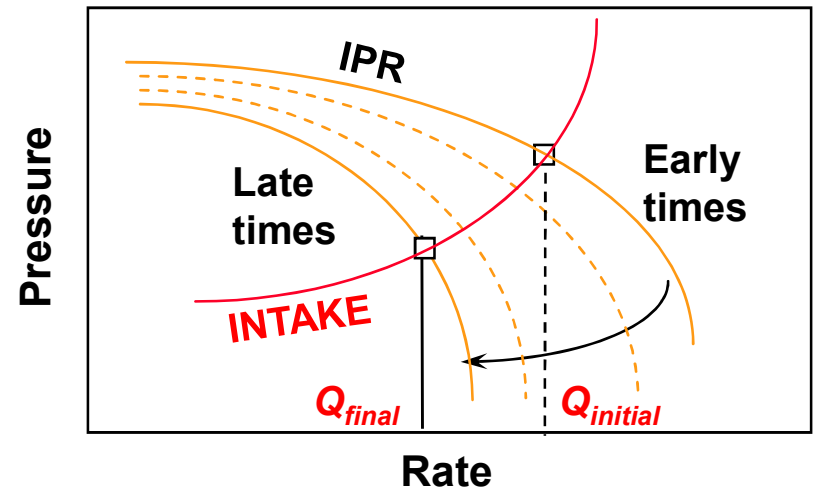
Need to improve the least permeable medium:



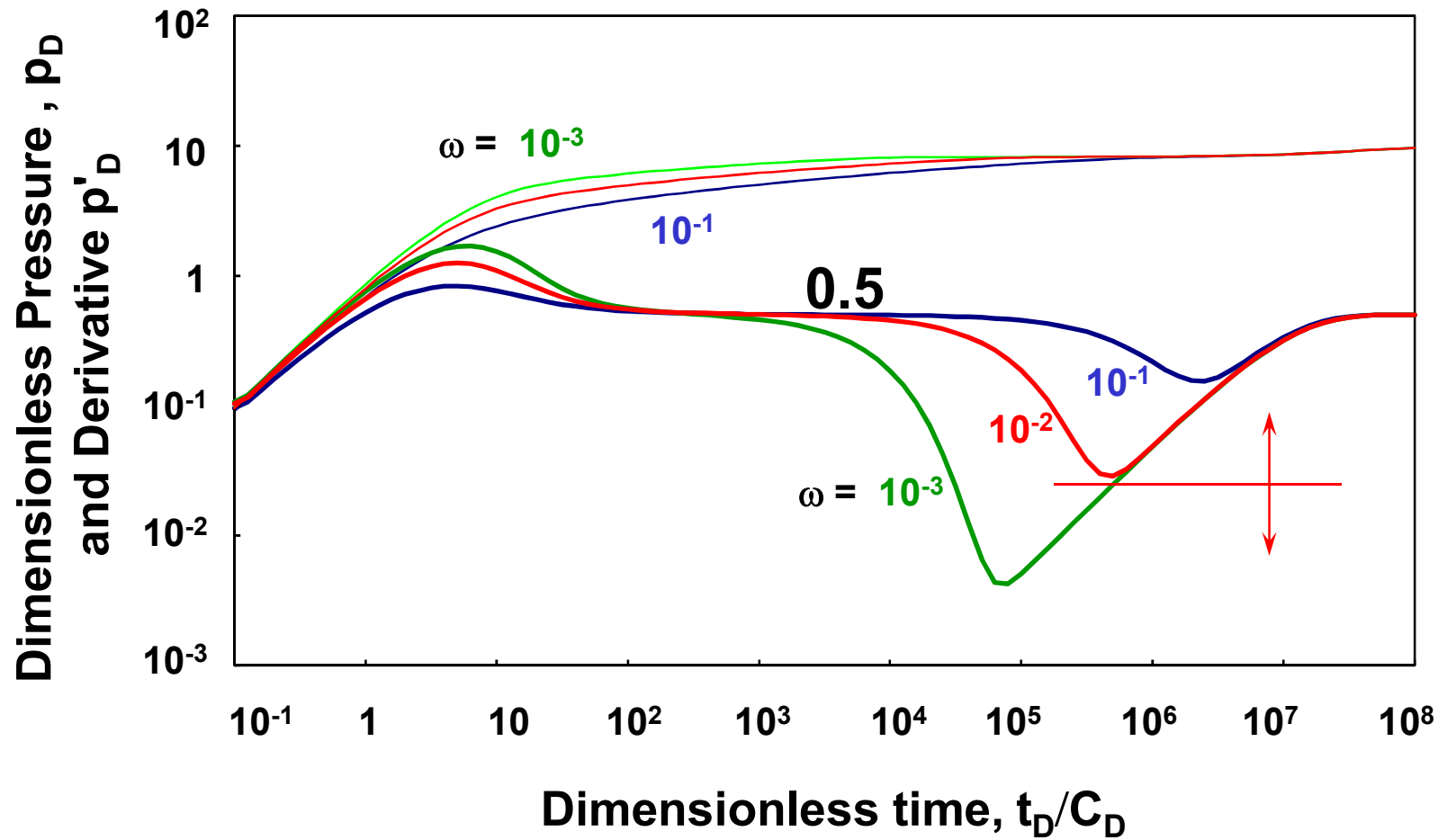
No improvement



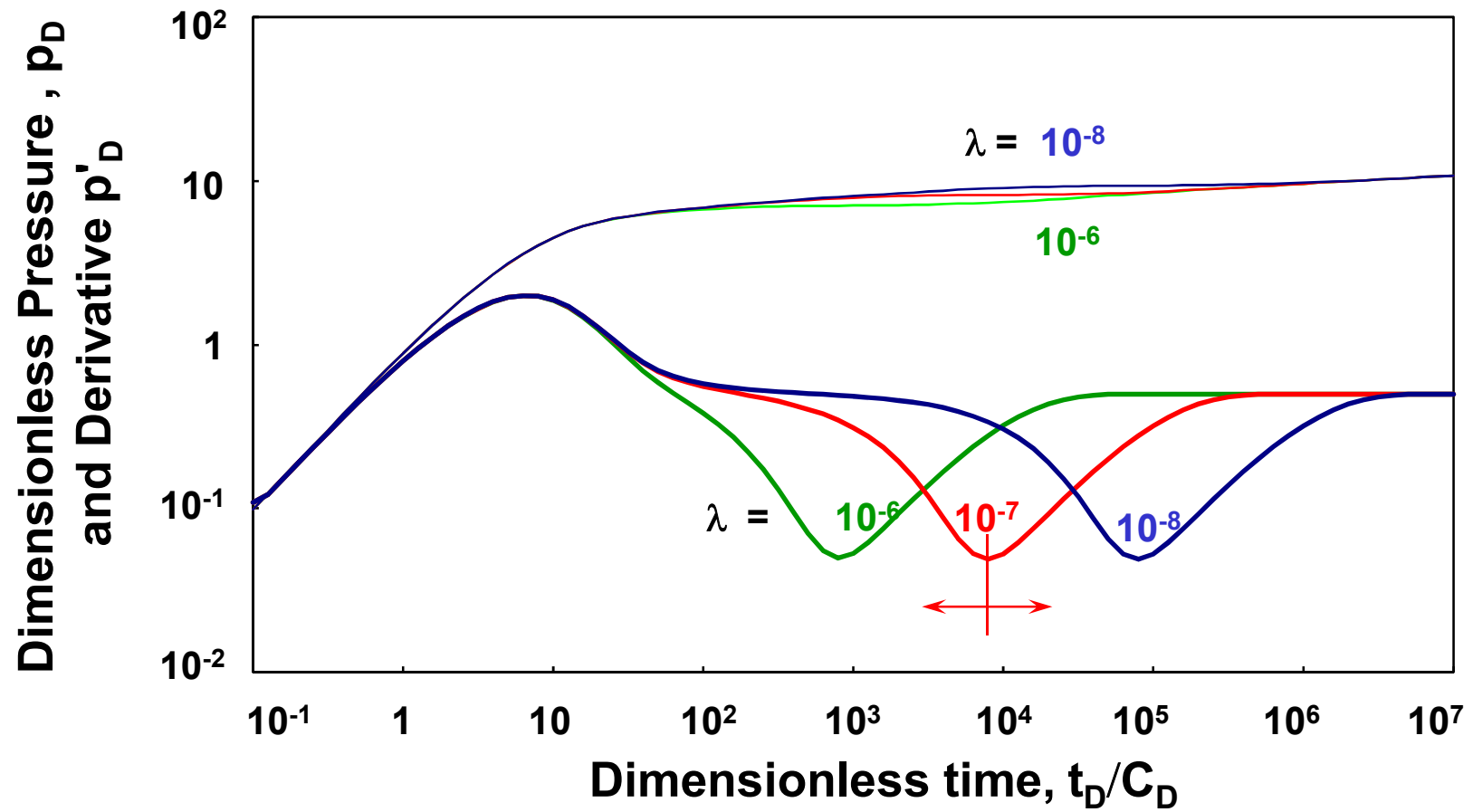
Significant improvement



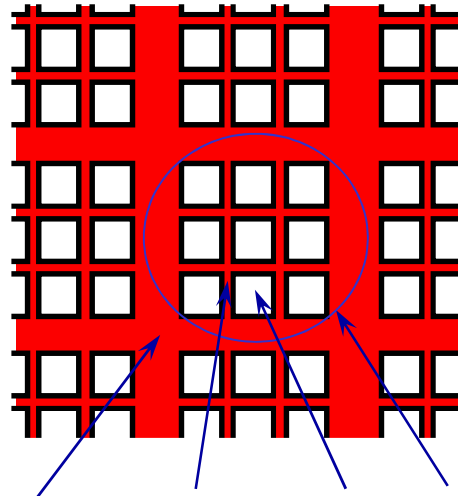
INFLUENCE OF ω



INFLUENCE OF λ

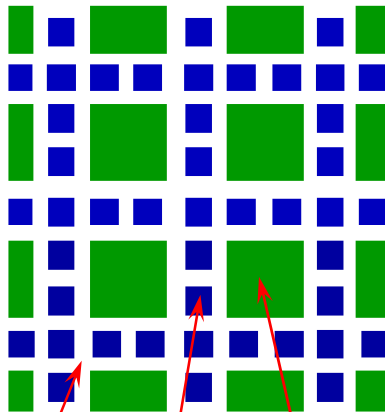


TRIPLE POROSITY RESERVOIR BEHAVIOUR



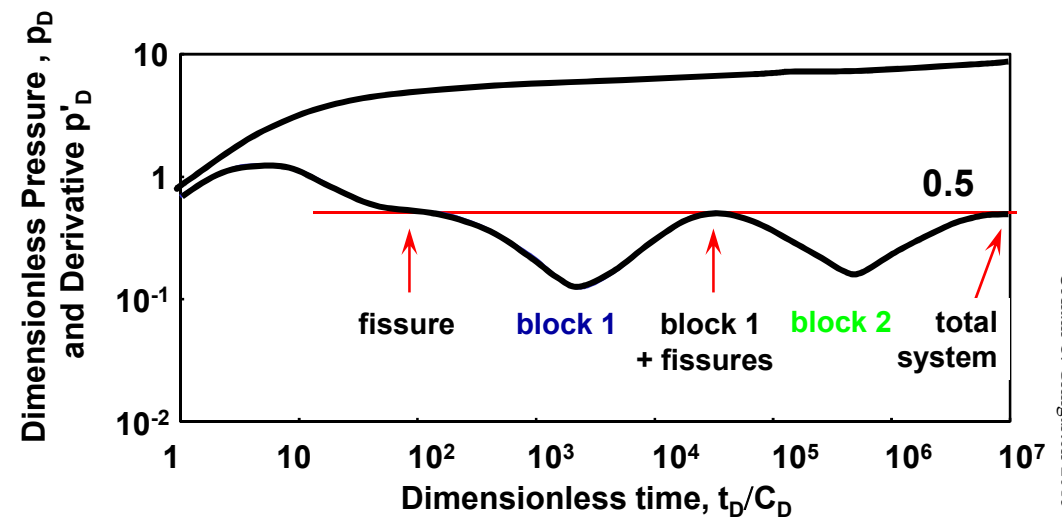
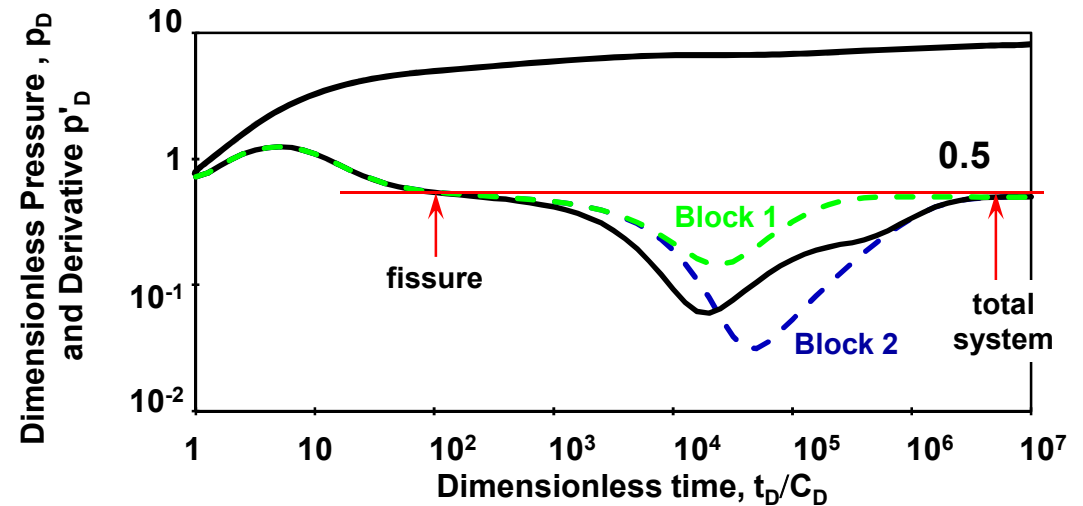
OR

fissure microfissure block 1 block 2
Fissured matrix blocks



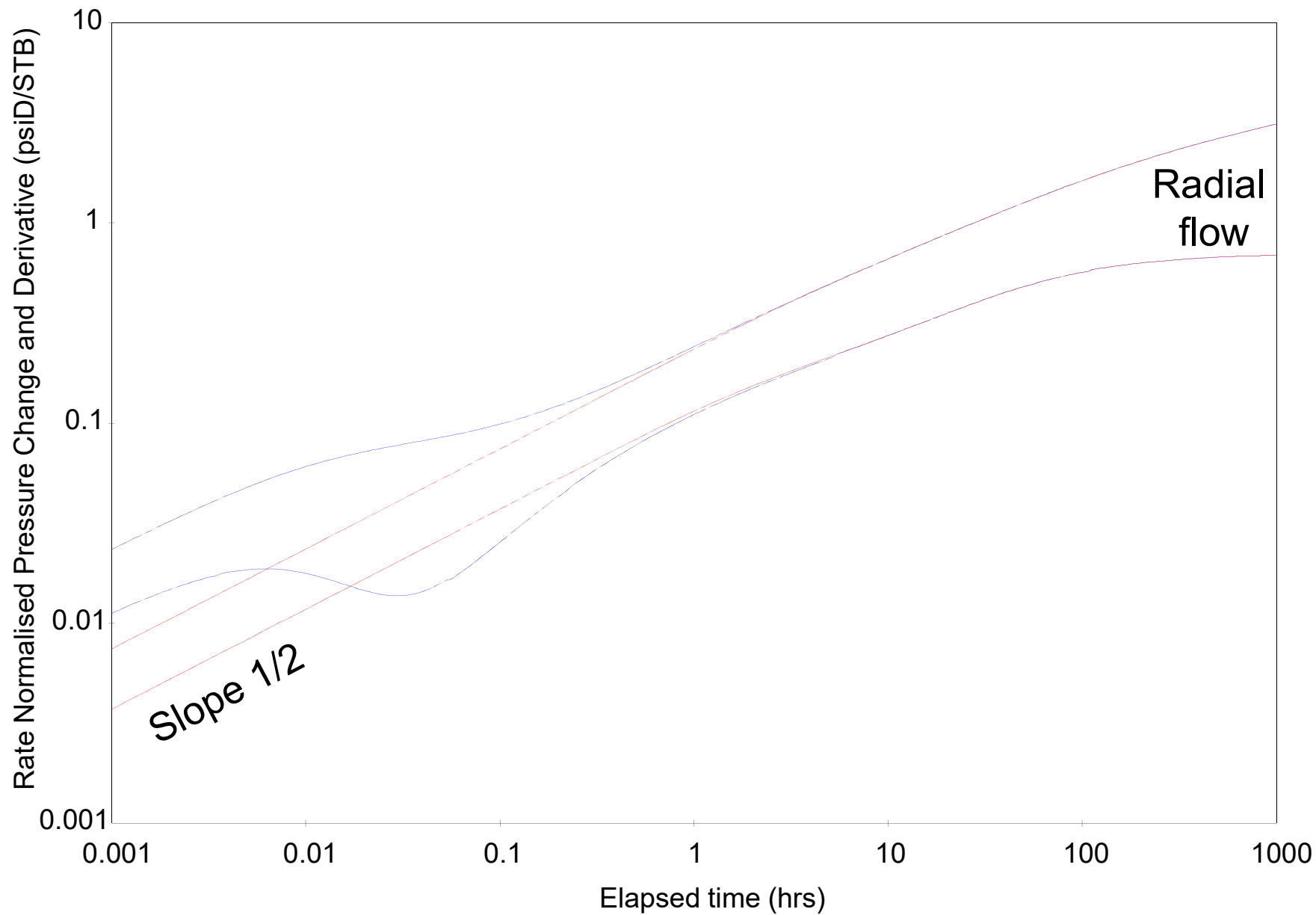
fissure block 1 block2

Two block sizes

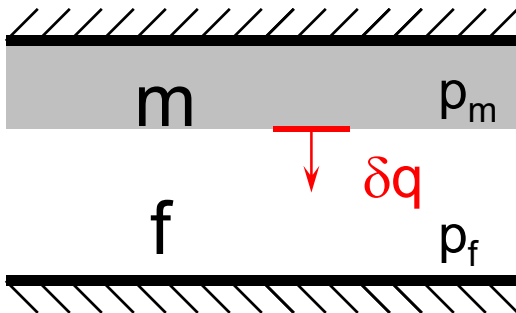
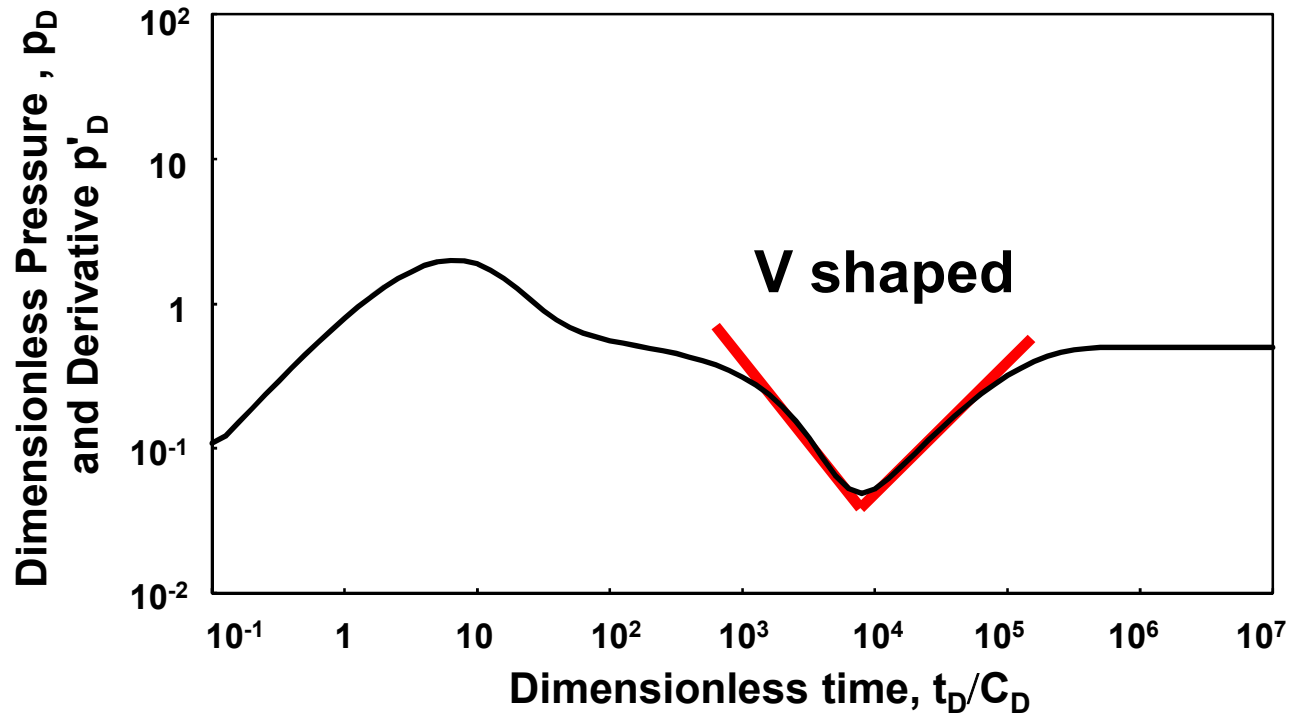


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FRACTURED WELL



RESTRICTED INTERPOROSITY FLOW



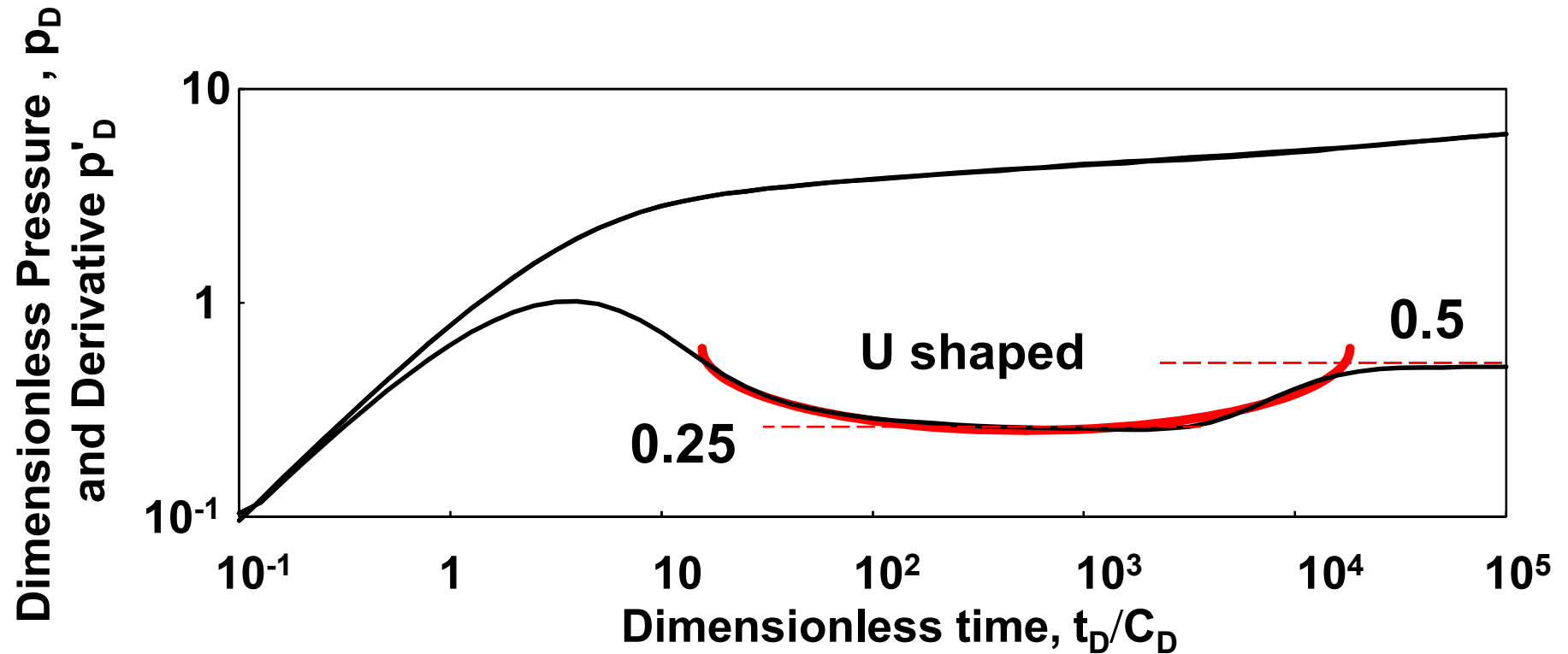
“Warren & Root” (Soc. Pet. Eng. J., Sept. 1963) or
“Pseudo-steady state interporosity flow” solution

$$\delta q = \alpha \frac{k_m}{\mu} (p_m - p_f)$$

Interporosity flow / unit interface area / unit time
Independent of block shape

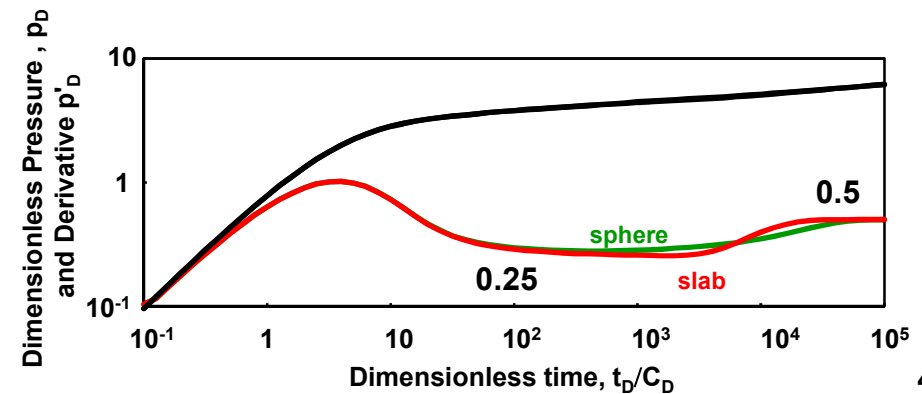
Barenblatt and Zeltov Soviet Physics Doklady (1960) Vol.5

UNRESTRICTED INTERPOROSITY FLOW



“Transient interporosity
flow” solution

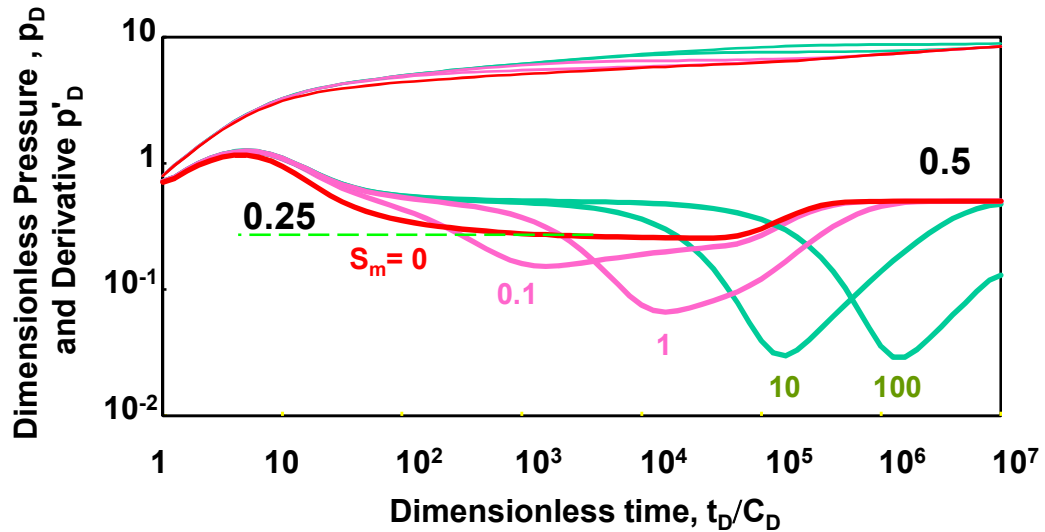
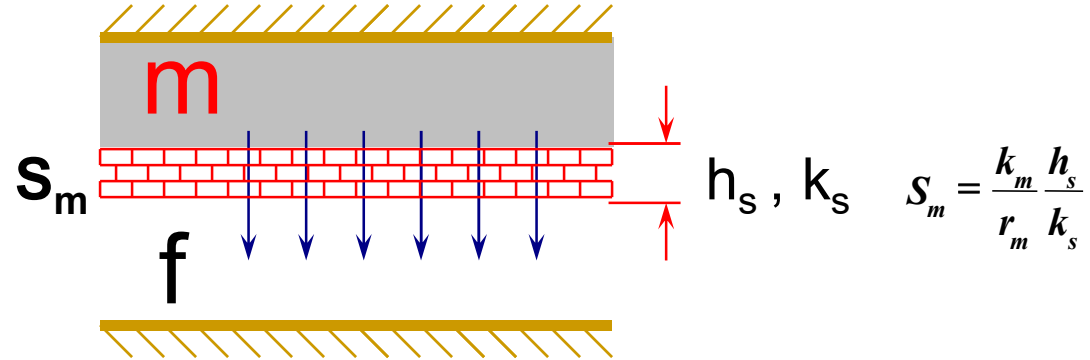
Dependent of matrix block shape



INTERPOROSITY SKIN

Moench Water Resour. Res. 20(7) July 1984

Cinco-Ley, Samaniego V. and Kucuk SPE14168 60th ATCE Las Vegas (Sept 1985)



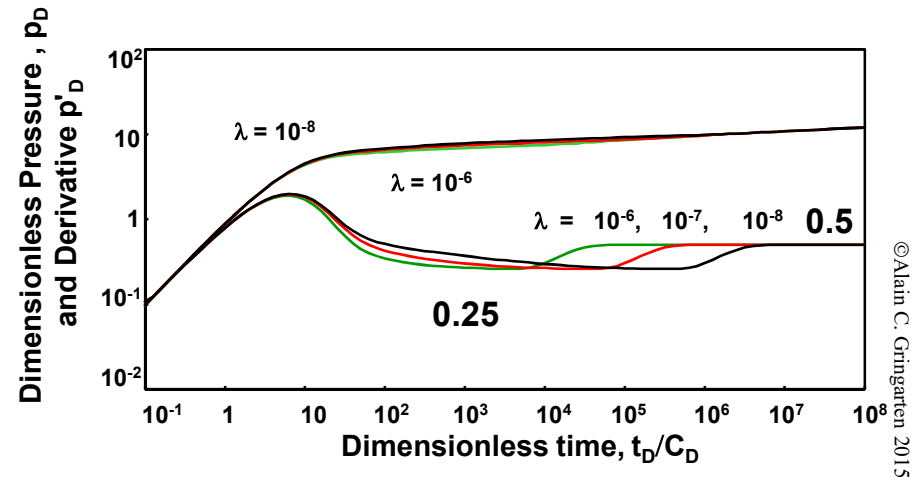
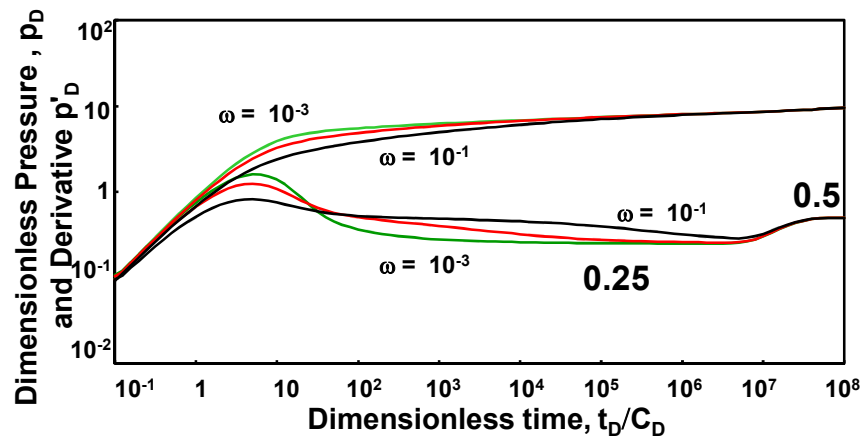
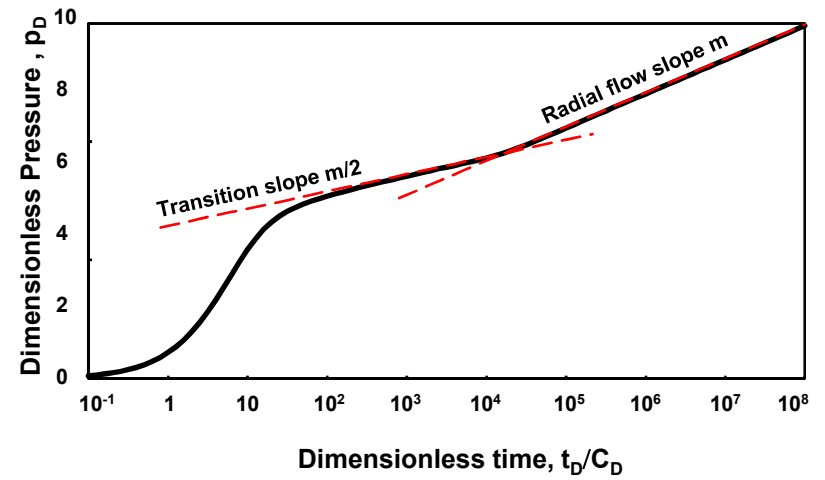
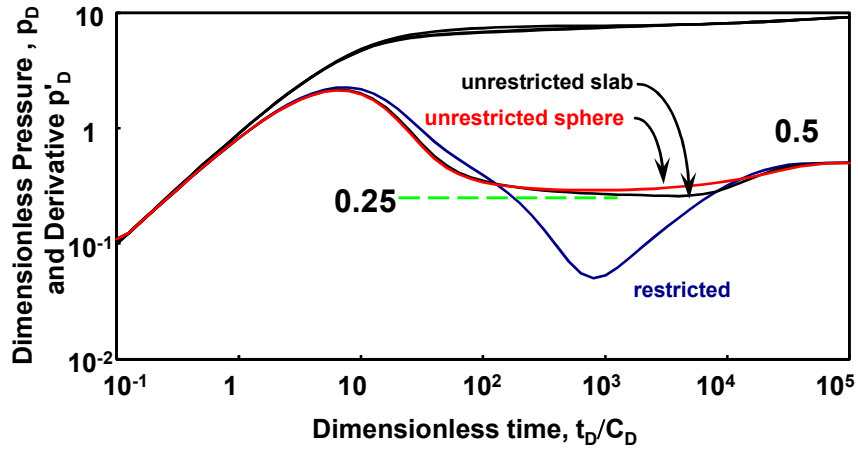
Warren and Root

pseudo-steady-state
interporosity flow solution

Transient interporosity flow solution

$$\lambda = \frac{12}{h_s^2} r_w^2 \frac{k_s}{k_f} \quad (\text{does not give access to the matrix block size})$$

UNRESTRICTED INTERPOROSITY FLOW



Drawdown Type Curves for a Well with Wellbore Storage & Skin, in a Reservoir of Infinite Extent with Double Porosity Behaviour (Unrestricted Interporosity Flow)

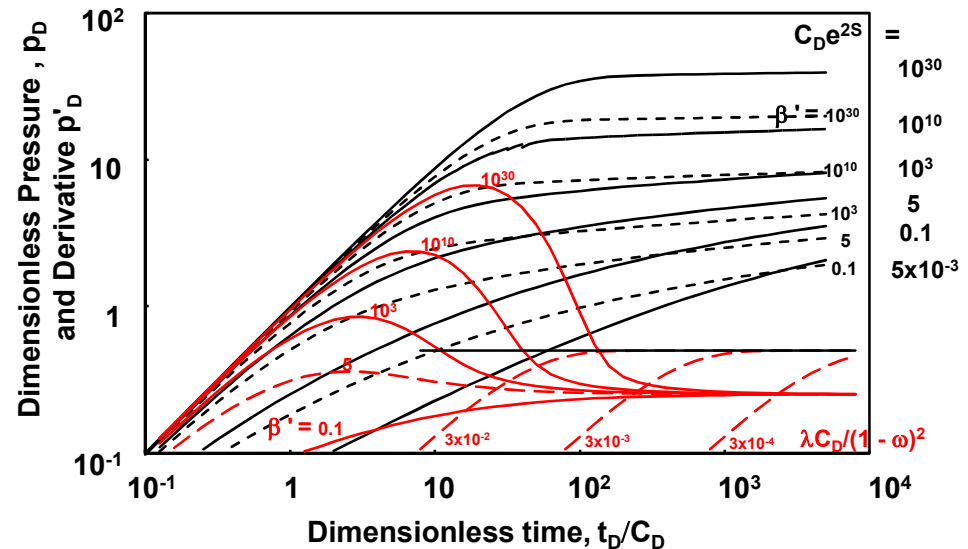
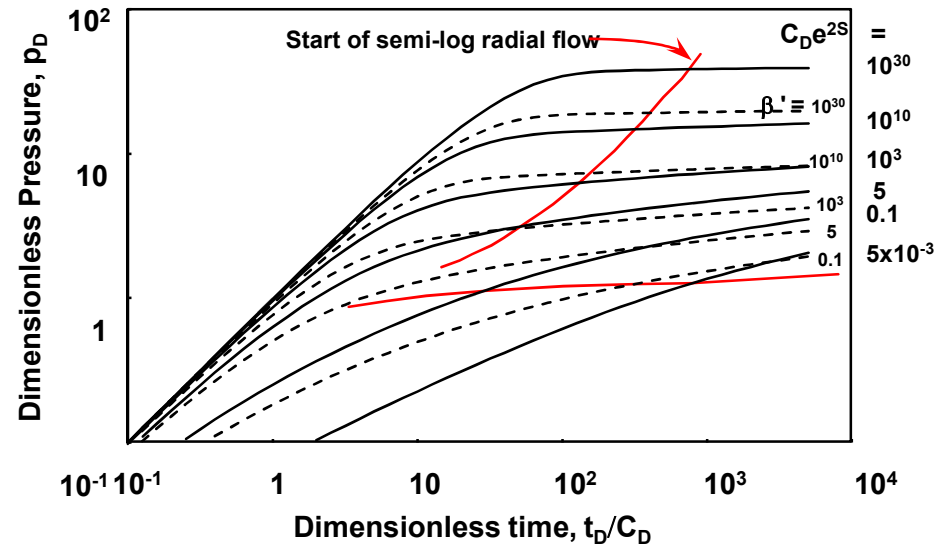
$$\beta' = \delta' \frac{(C_D e^{2S})^{f+m}}{\lambda e^{-2S}}$$

Slab matrix blocks:

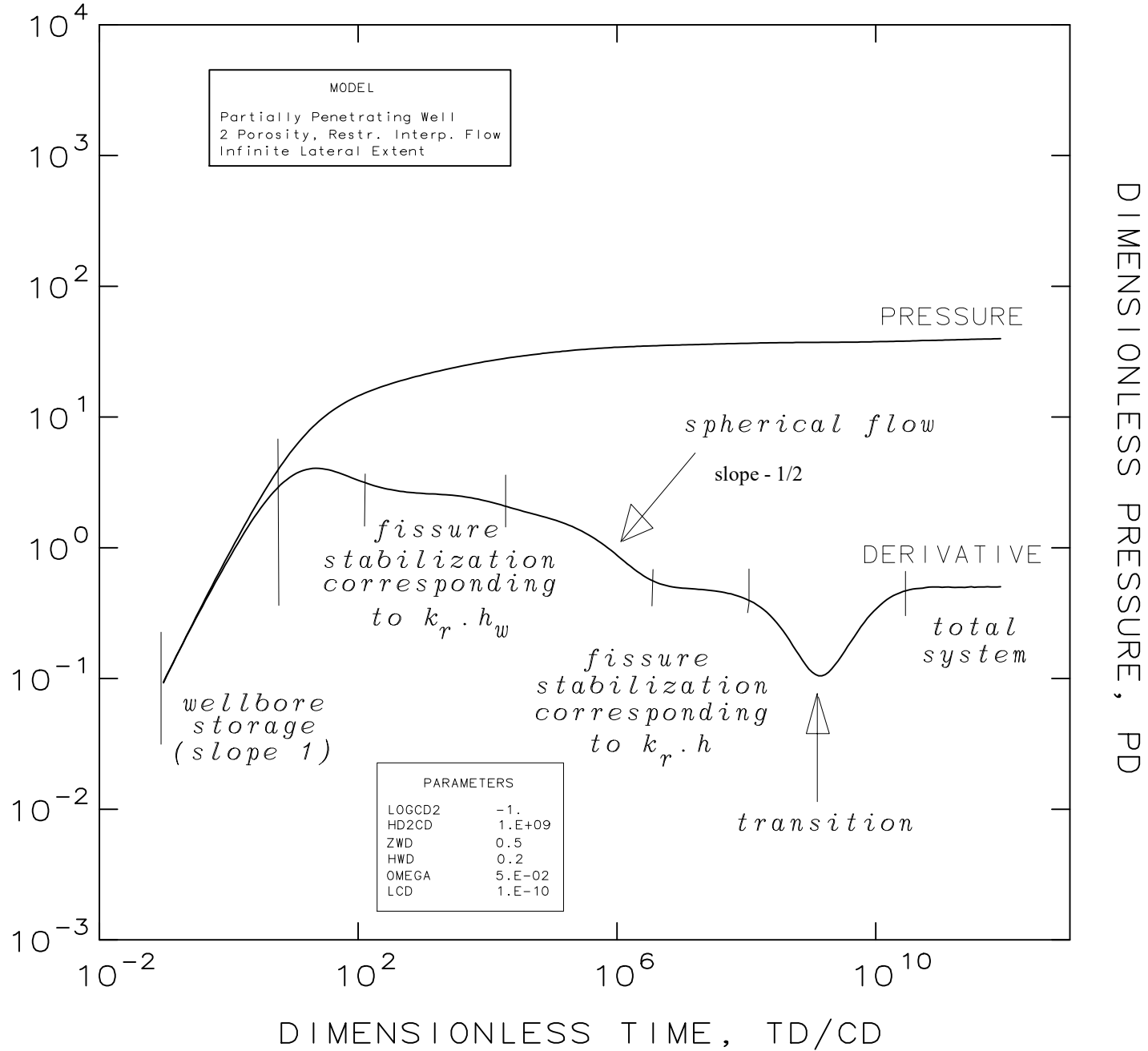
$$\delta' = 1.89$$

Sphere matrix blocks:

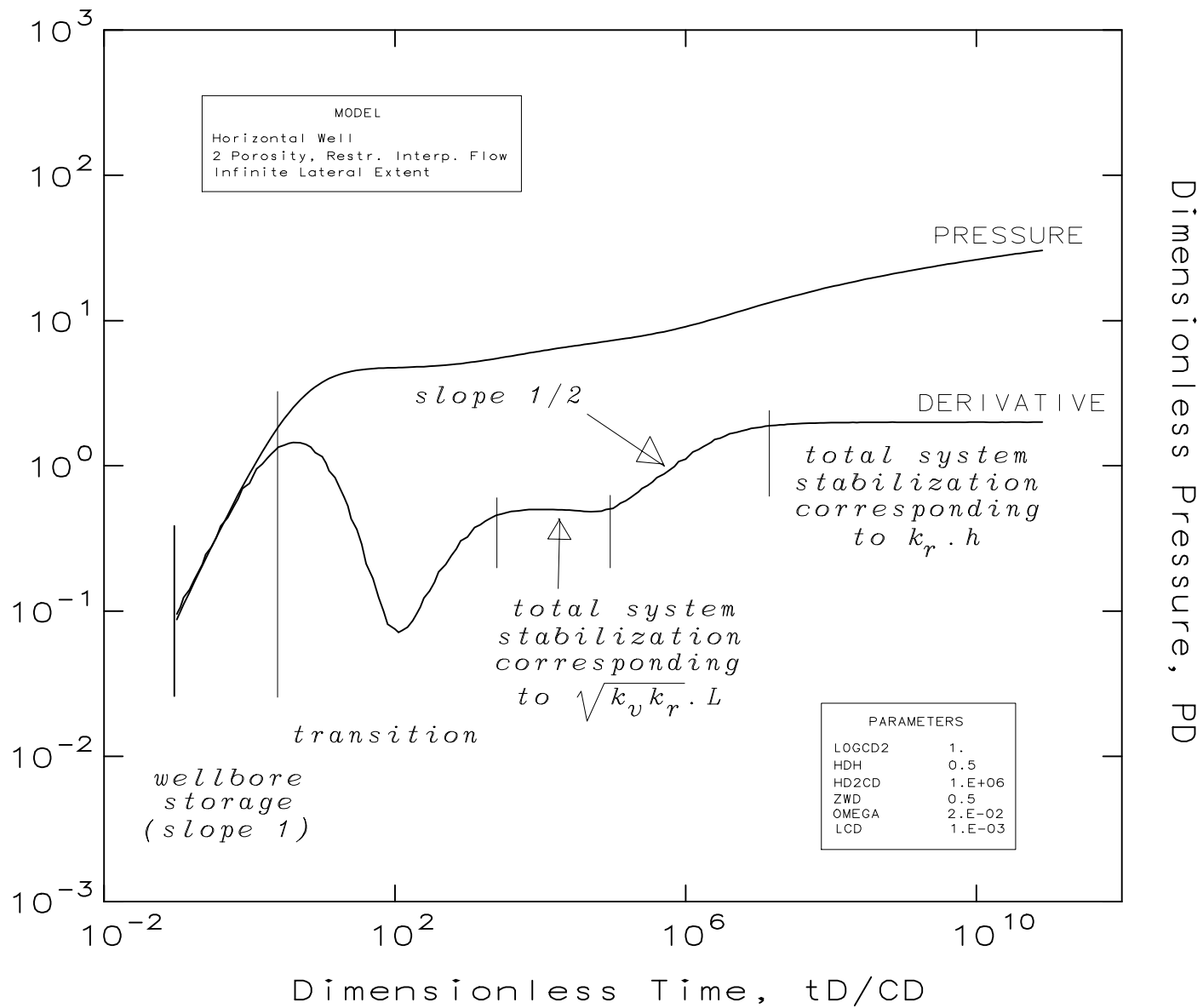
$$\delta' = 1.05$$



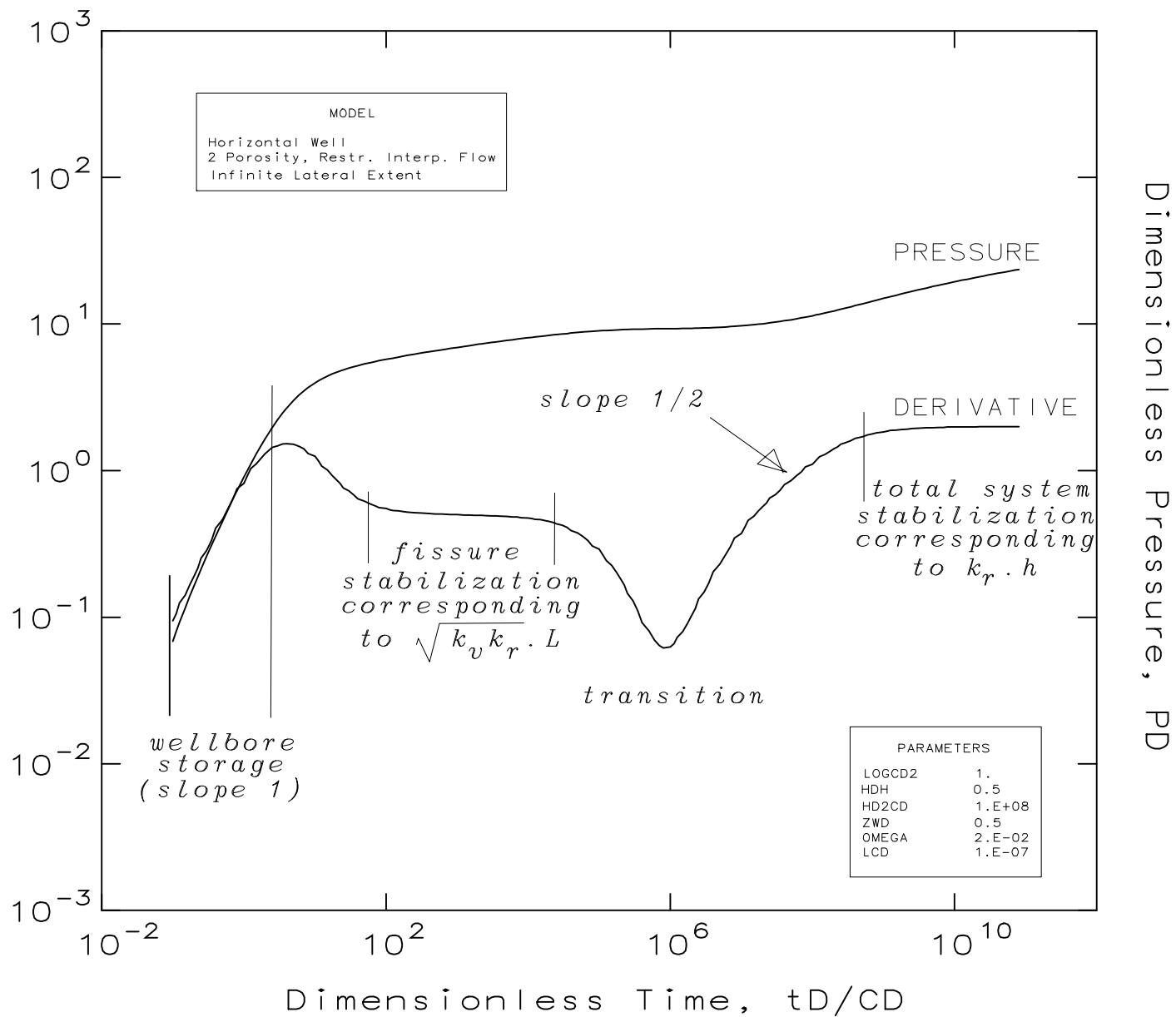
WELL WITH LIMITED ENTRY



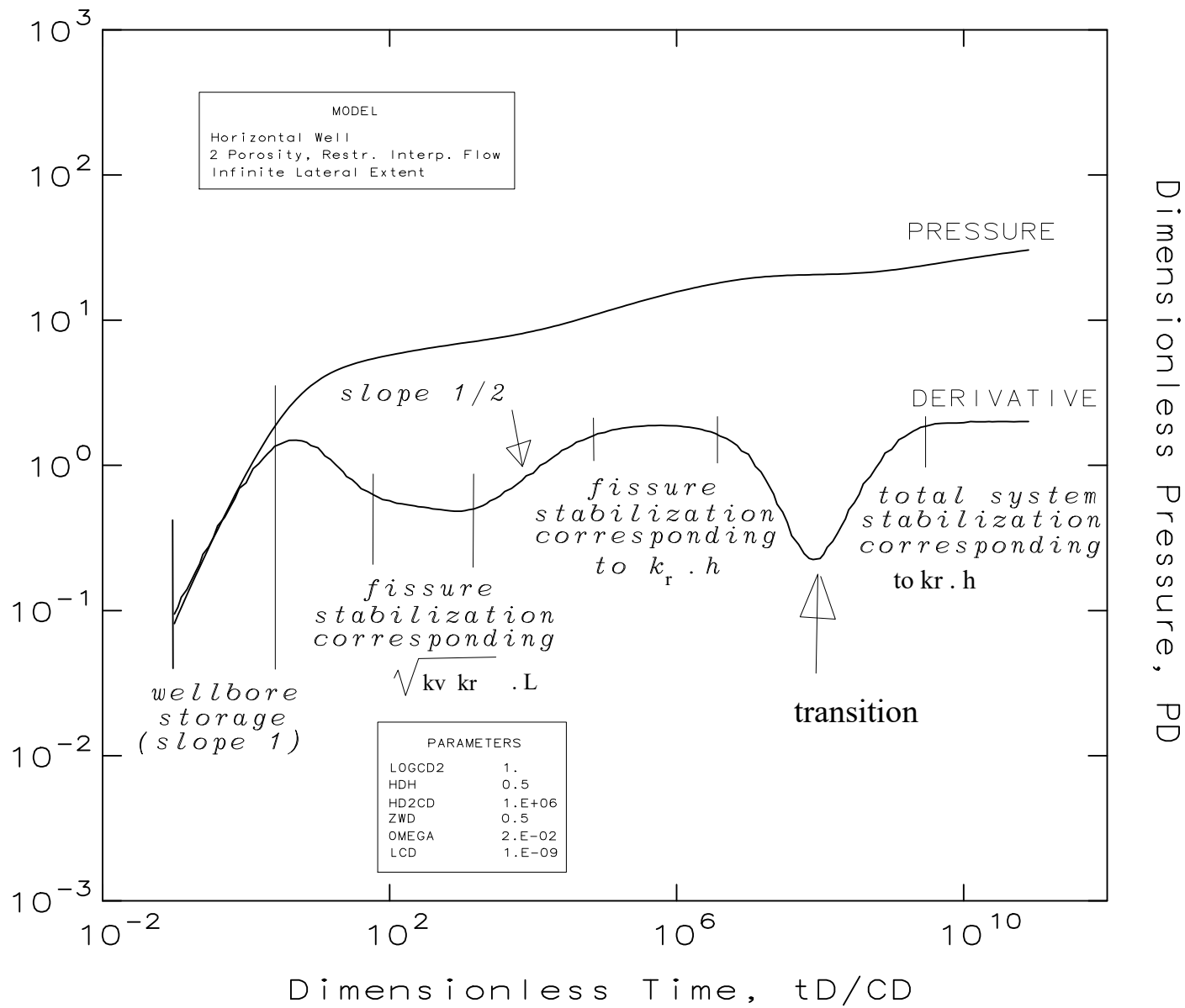
HORIZONTAL WELL



HORIZONTAL WELL



HORIZONTAL WELL



COMPOSITE BEHAVIOUR

